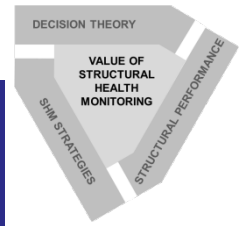


# Thermal monitoring of dams and levees

**Krzysztof Radzicki** – Cracow University of Technology (Poland)

**Bonelli Stephane** - IRSTEA (France)

Barcelona, 2016



# Statistics of damming structures collapses due to internal erosion processes

## Earth dams

(World, several years)

Foster, 2000

46%

## Flood protection dikes / levees

(Poland, flood 2010r)

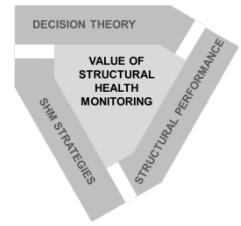
Kledyński et al. 2012

30%

## Collapse of dike in Cracow Bend of Vistula (2010)

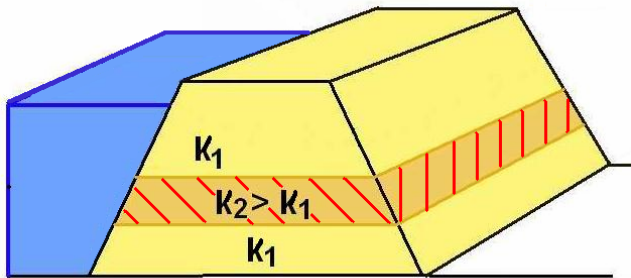
- The failure occurred at night
- No recent signs of danger





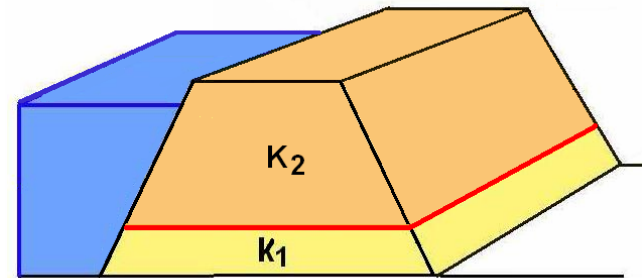
# Internal erosion

## SUFFUSION

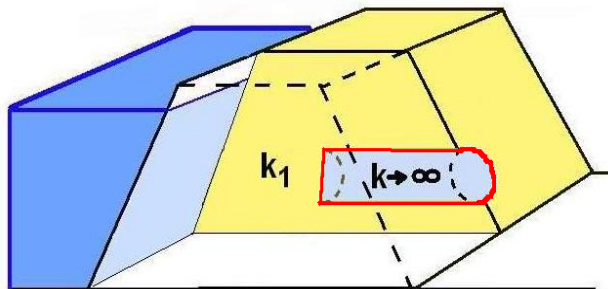


Risk of piping

## CONTACT EROSION

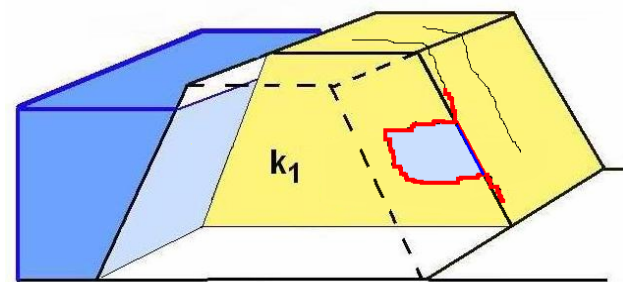


## BACKWARD EROSION

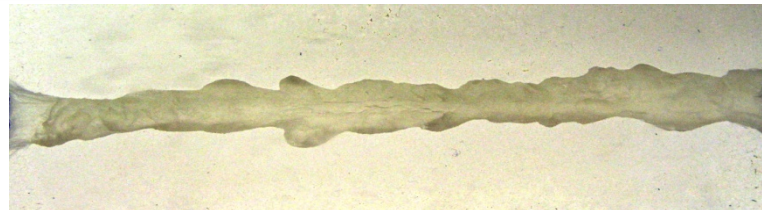


High risk of piping

## CONCENTRATED LEAKS



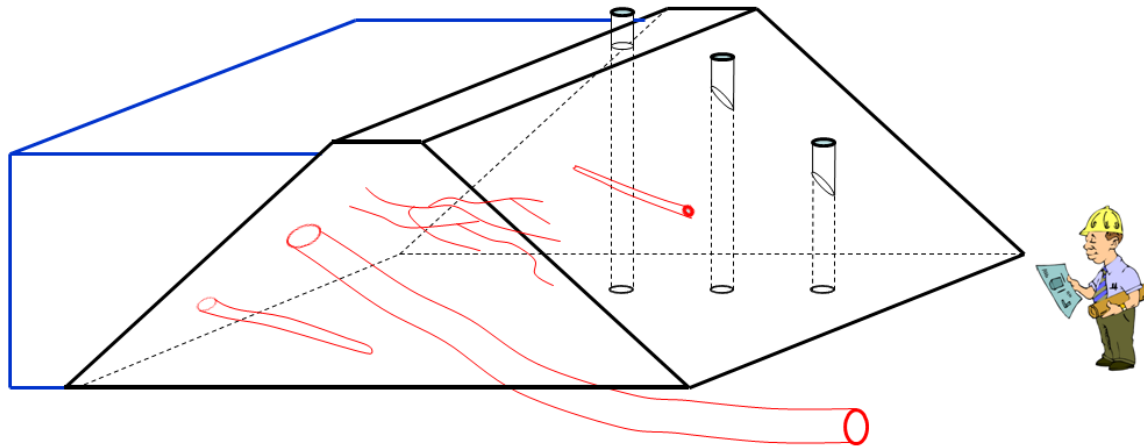
# PIPING



# The problem of piping detection and monitoring

Visual inspections, spot geotechnical studies, geophysical surveys, spot sensor monitoring (if it exists),

- ✓ are not sufficient to reliably detect and assess the development of erosion processes
- ✓ especially in the early stages of their development,
- ✓ and especially during the floods to keep levees safe!



*„The frequency of piping failures is significantly higher on first filling and early in the life of the dam.”*

FOSTER et al.. (2000 - The statistics of embankment dam failures and accidents.)

*„In the majority of failures, breaching of the dam occurred within 12 h from initial visual indication of piping developing, and in many cases this took less than 6 h”.*

FOSTER et al.. (2000 - A method for assessing the relative likelihood of failure of embankment dams by piping.)

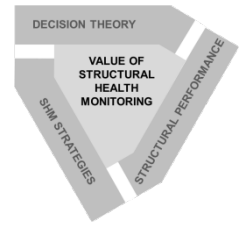
# The problem of reliable condition assessments and monitoring of EARTH DAMS

- The necessity to minimize the probability of dam collapse
- Aging of dams
- Internal erosion is one of the main threats to the safety of dams
- Shortage of decision support tool for the identification of sections requiring renovation
- Assessment of dams state based on spot measurements

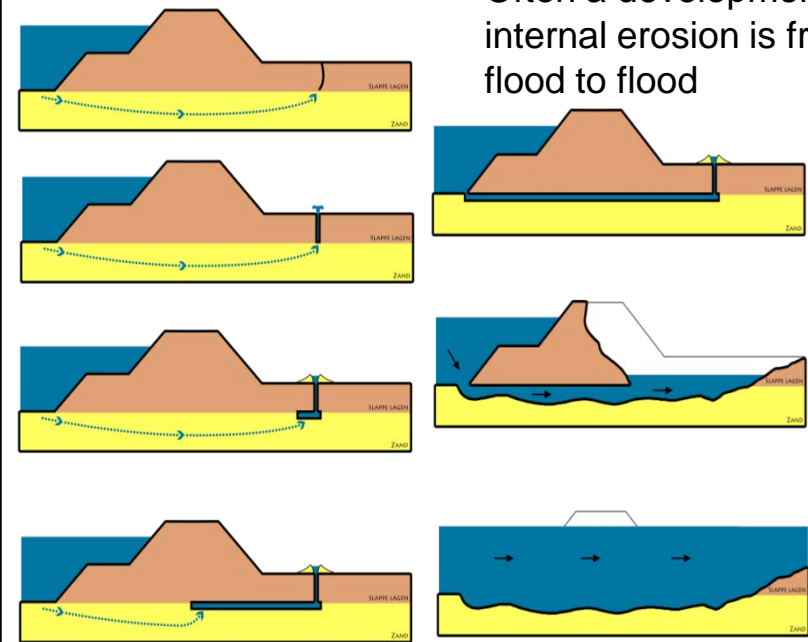
100m high Teton dam (1976) – collapse in 3 hours due to piping



## The problem of reliable condition assessments and monitoring of LEVEES

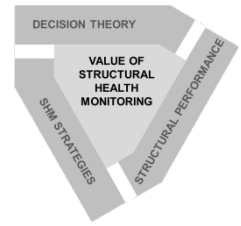


- The necessity to minimize the probability of disaster of dikes protecting valuable areas particularly urban and industrial
- Often poor condition of existing levees
- Shortage of methods for identification of vulnerable sections, especially in the early stages of development of erosion processes, especially the piping
- Shortage of diagnostic tools enabling automatic detection of internal erosion threats during flood defense
- Shortage of methods to assess the most vulnerable sections of levees among all the sections where leakages were detected
- Shortage of decision support tools for identification of critical sections of levee after the flood that require immediate repair
- Condition assessment of the levee based on spot, usually geotechnical measurements



Often a development of internal erosion is from flood to flood

ICOLD bulletin B164 (2013)



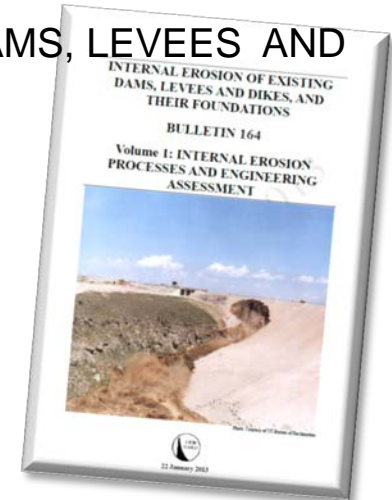
# EWG ICOLD recommendations

## European Working Group on Internal Erosion of ICOLD

ICOLD's Bulletin no 164 (2013): „INTERNAL EROSION OF EXISTING DAMS, LEVEES AND DIKES, AND THEIR FOUNDATIONS”

VOL.1 INTERNAL EROSION PROCESSES AND ENGINEERING ASSESSMENT

*<Many less direct means of detecting seepage are now available. The most promising is temperature measurement which can be used to infer localized flow. Fiber optic cables facilitate data collection and make it possible to cover large parts of the dam. Remote sensing options also offer great potential in detecting whether the seepage has caused erosion. These will be discussed in detail in Volume 2 of the Bulletin.>*

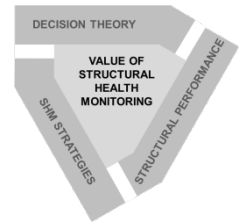


Jean-Jacques FRY (2012), the chairman of ICOLD European Working Group on Internal Erosion - 80th ICOLD annual meeting in Kioto

PAPER : „HOW TO PREVENT EMBANKMENTS FROM INTERNAL EROSION FAILURE?”

*<In our opinion, Distributed Fibre Optic Temperature measurement is the best method .... Remote control monitoring of temperature by fibre optic is the only method available for practical application, which has been used successfully during the last 10 years during the last 10 years in Germany, Sweden and France>*

*<The IJkdijk-piping tests clearly demonstrate the reliability and the capabilities of the fiber optic system to detect the early stage of a piping process.>*



# Coupled heat and water transport

## DIFFUSION-ADVECTION EQUATION

$$C_{\ominus} \frac{\partial T}{\partial t} + C_f \bar{q} \frac{\partial T}{\partial x} - \lambda_{\ominus} \frac{\partial T}{\partial x^2} = 0$$

## SYSTEM NONDIMENSIONAL

$$\bar{q} = \text{const.}$$

$$\bar{x} = \frac{x}{L} \quad \bar{t} = t \frac{L^2}{D_{\ominus}} \quad D_{\ominus} = \frac{\lambda_{\ominus}}{C_{\ominus}}$$

$$\frac{\partial T}{\partial \bar{t}} + Pe \frac{\partial T}{\partial \bar{x}} - \frac{\partial T}{\partial \bar{x}^2} = 0$$

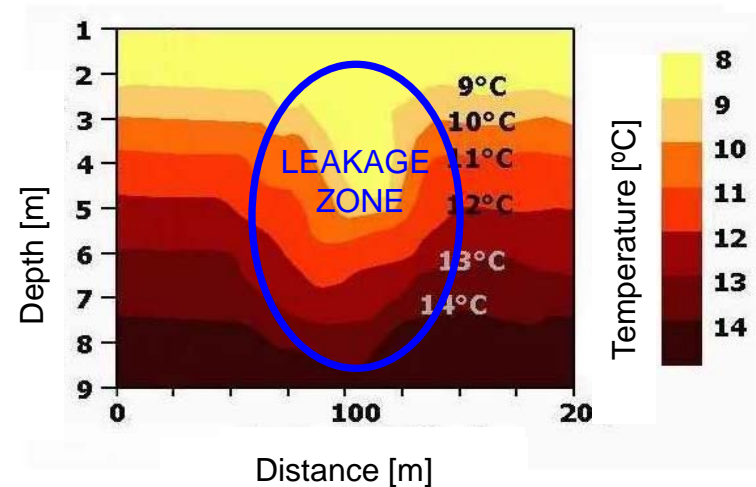
## Peclet number

$$Pe = \frac{\text{advection}}{\text{conduction}} = \frac{C_{\ominus} \bar{q} L}{\lambda_{\ominus}}$$

Conduction domination      Advection domination

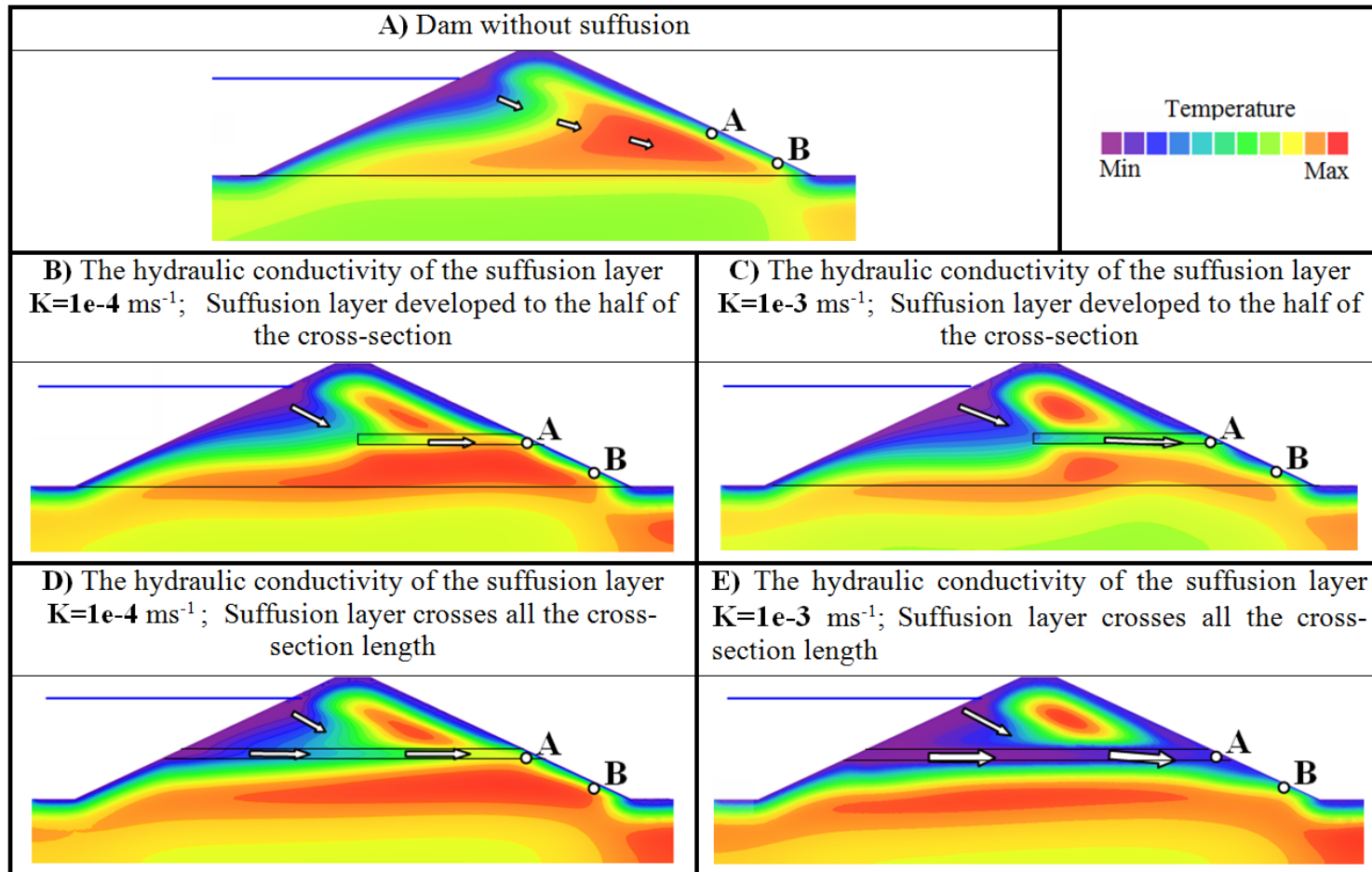
$$Pe < 1$$

$$Pe > 1$$





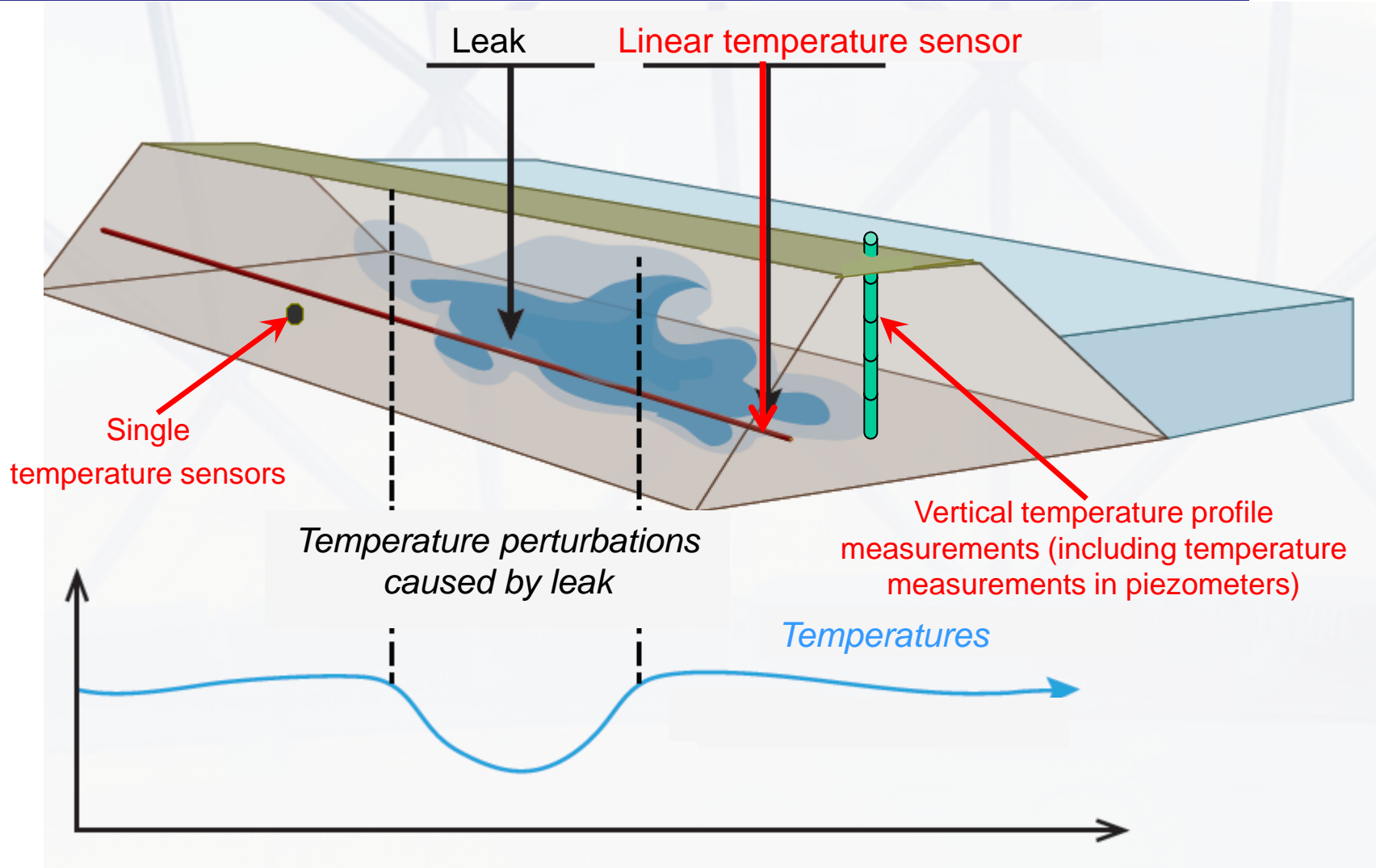
# Example of the impact of internal erosion development on the temperature field in the damming structure



Temperature fields of a dam cross-section registered at the same time instant for different lengths of suffusion layer and for different values of suffusion layer hydraulic conductivity.

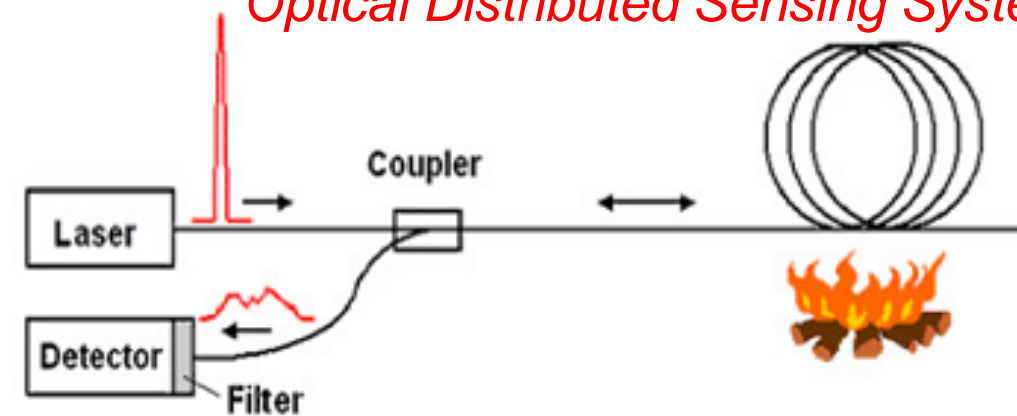
Radzicki and Bonelli (2012)

# Methods of temperature measurements

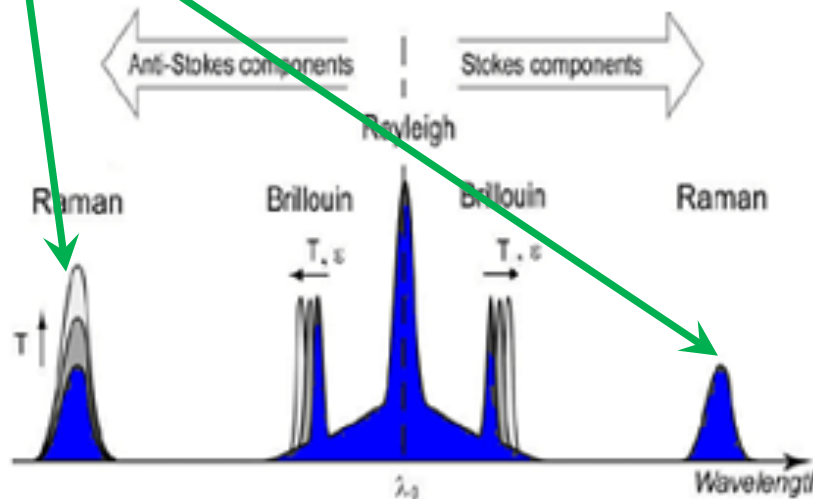


# Linear temperature sensors

## Optical Distributed Sensing Systems



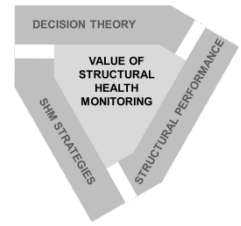
Spectral analysis of backscattered light



Fiber optic temperature sensing:

- Spatial resolution 1m
- Resolution  $\pm 0,1^{\circ}\text{C}$
- Measurement distance - up to 30km with one fiber optic cable

Optimal for installation on new damming constructions (dams, levees,.....), during renovations and assuming the decades-long application



# Problems with DFOTS application at existing structures

## COST OF APPLICATION

- Costly earthworks of cable installation
- Costly technology for short distances of measurements  
and/or particularly for temporally leakage or erosion problem monitoring  
(costly sensing head - DTS unit)

## SAFETY PROBLEMS OF THE STRUCTURE

- Earthworks affect the body or the foundation of the structure.  
Foundation structure must be rebuilt very carefully.
- In the case of high water level in the body of damming structure  
the risk of fiber optic cable installation can be too high to accept  
this monitoring solution application

# Linear temperature sensors

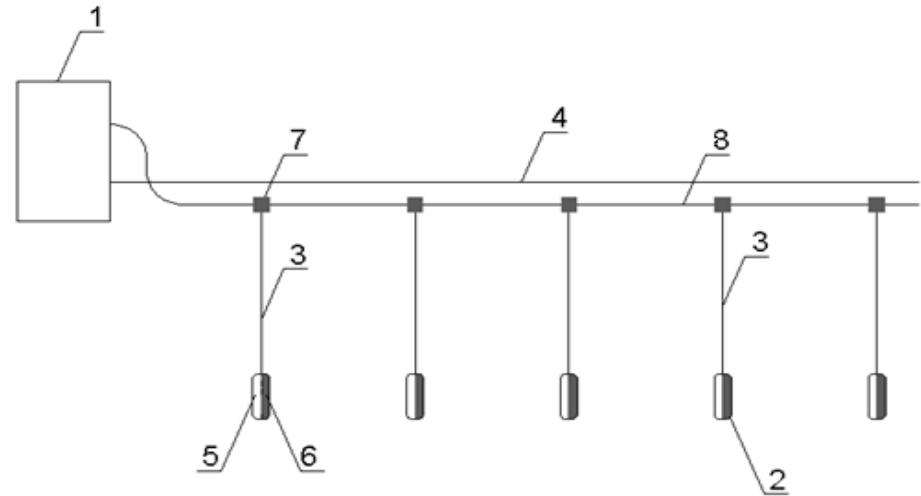
## *MPointS*

*Driving Multi Points Sensor to use for passive or/and active quasi continuous thermal monitoring*

MPointS are mounted without an excavation by inserting successive sensors in a series, one after another without necessity of the earthworks.

MPointS can be installed along the damming structure particularly at its downstream toe instead of fiber optic cable.

Can be installed much deeper than fiber optic cable



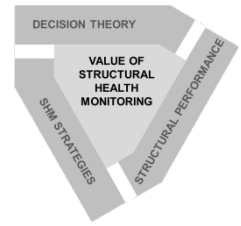
Particularly useful for monitoring of existing dams and embankments. Much cheaper and easier for installation than fiber optics.

Optimal for use for temporary monitoring (up to several years) of leakages and internal erosion processes in order to optimize decisions about necessity of renovation and/or about its range.

# Linear temperature sensors

## *MPointS - installation*



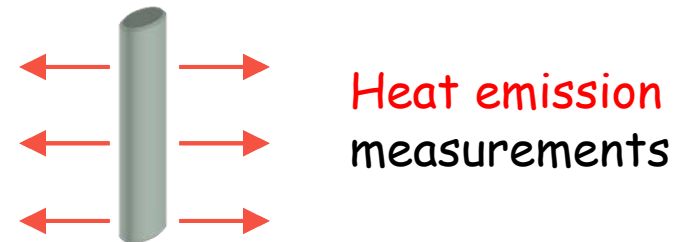


# Passive and active thermal monitoring

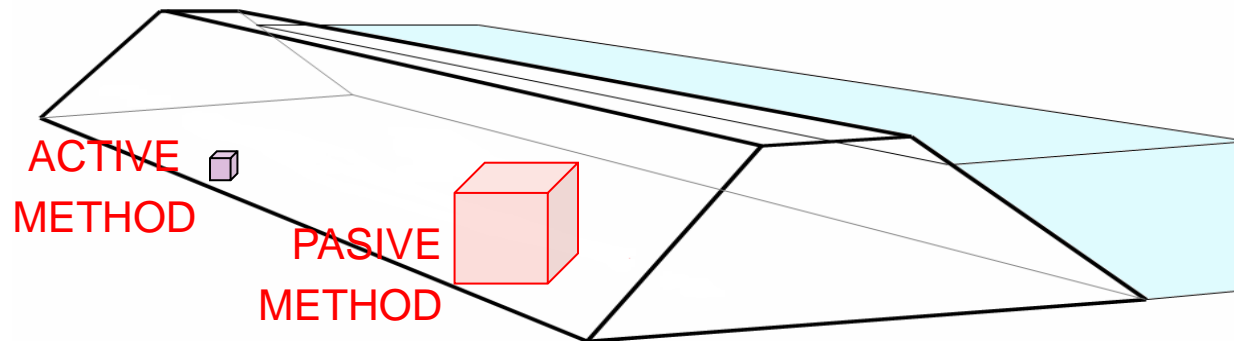
## PASSIVE METHOD



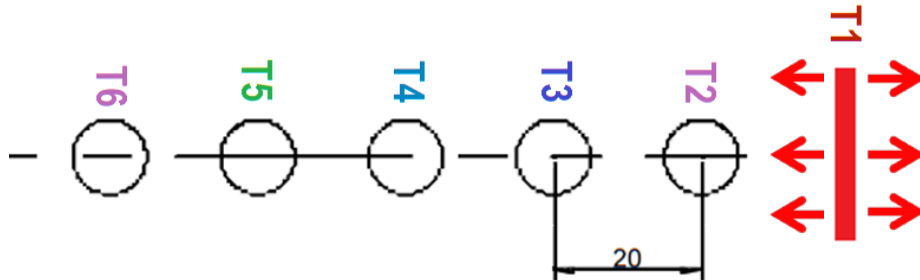
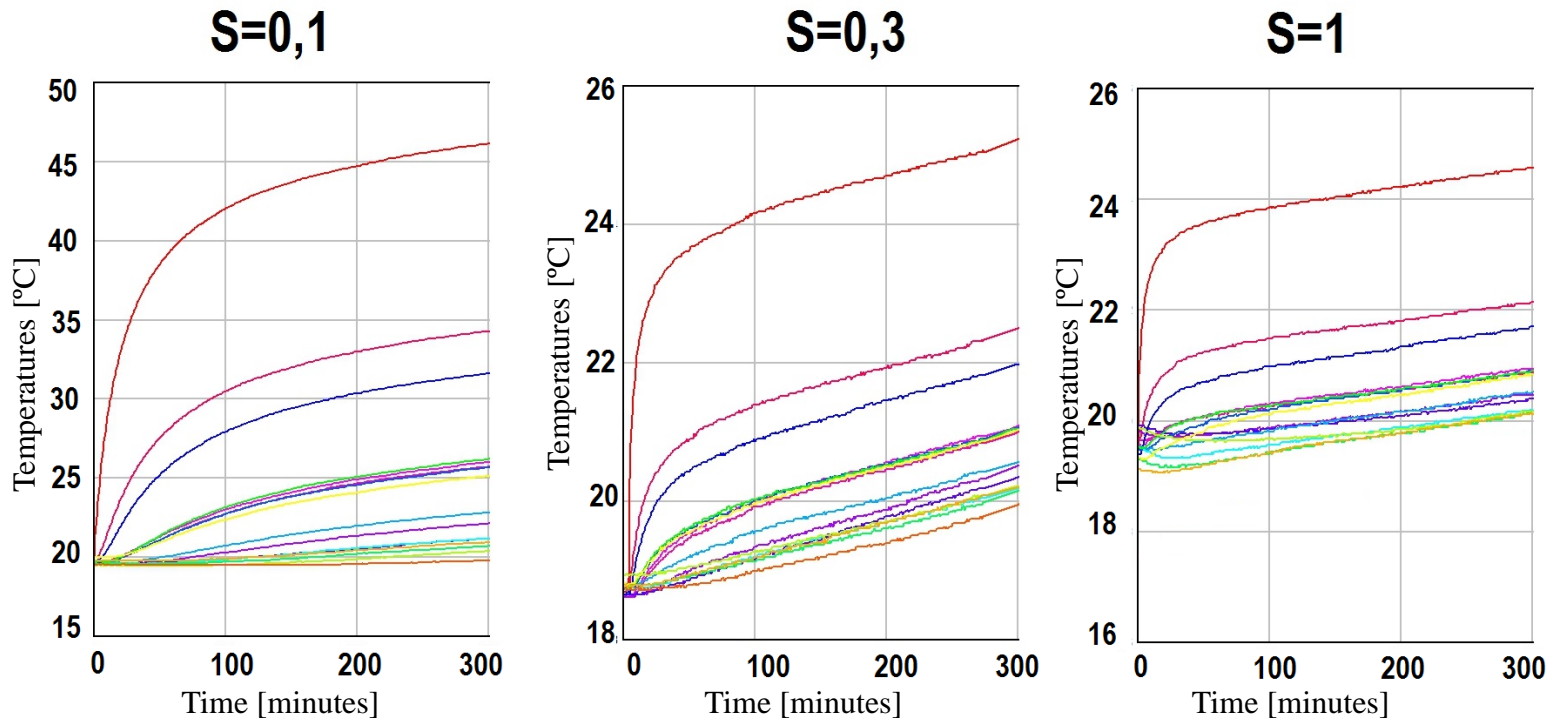
## ACTIVE METHOD



## Schematic extent of the leak detection zone for spot measurements



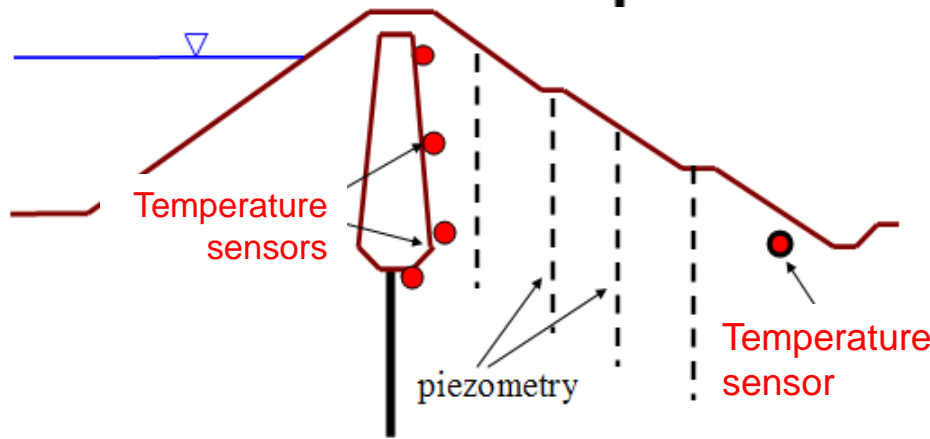
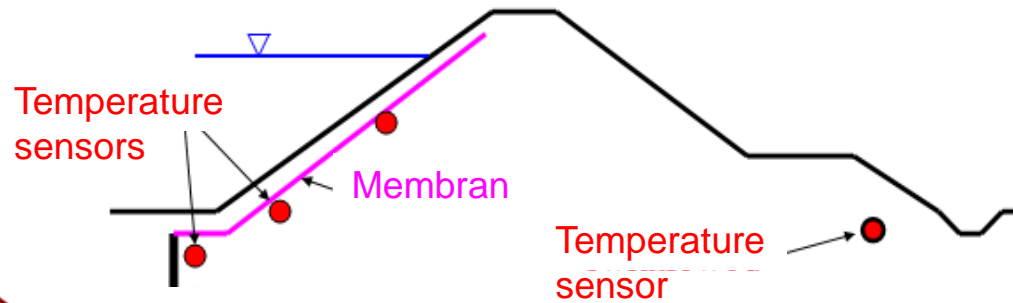
# Active method – laboratory test of heat distribution for different moisture values



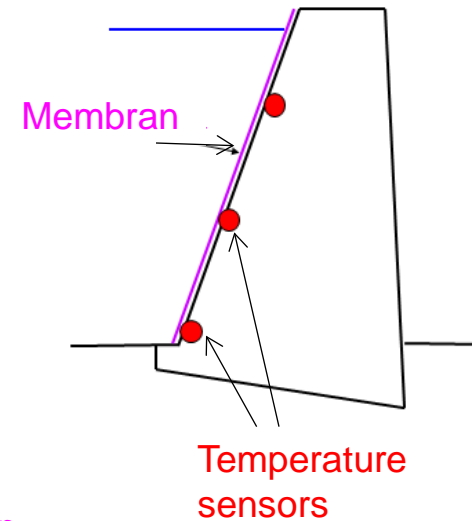


# Location of linear temperature sensors

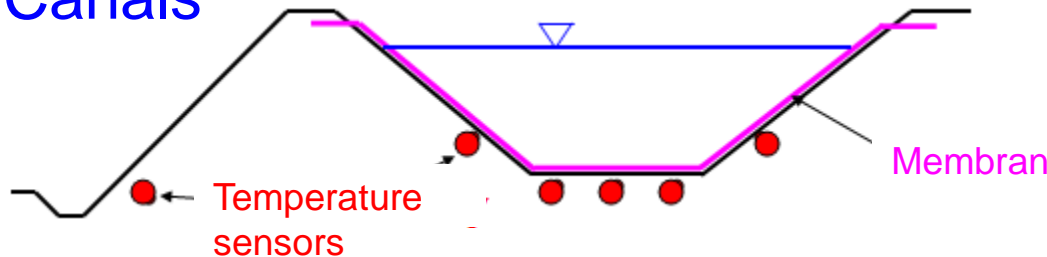
## Earth dams and levees

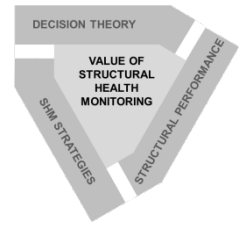


## Concrete dams



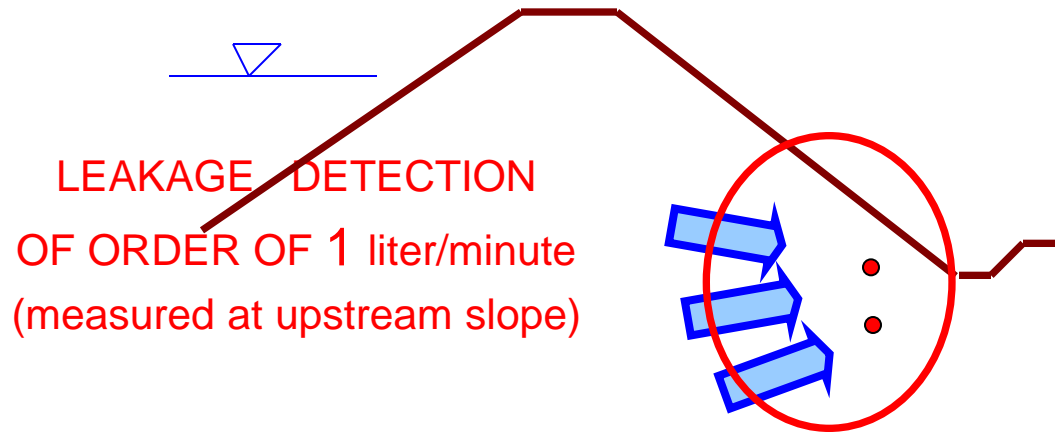
## Canals



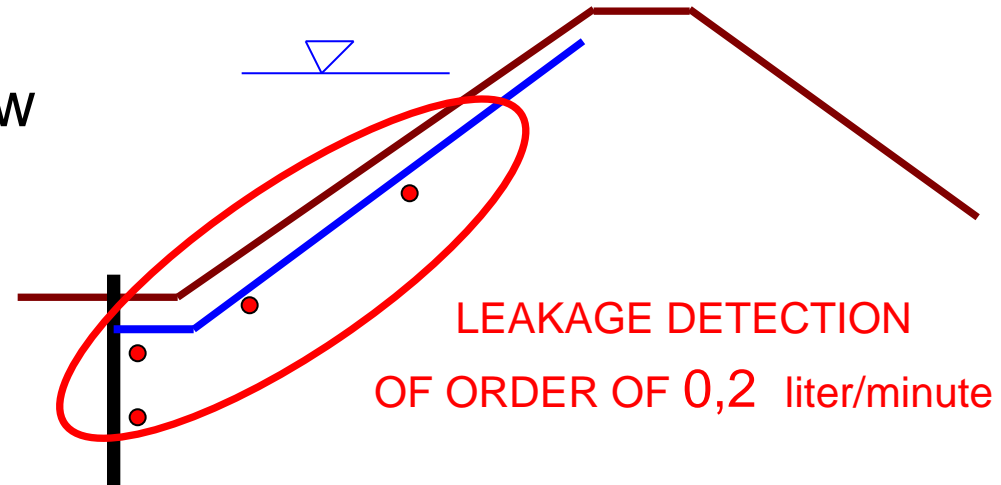


Research in real scale confirmed that thermal monitoring is reliable and precise tool and allows for early detection of leakages and internal erosion

Fiber optic located in downstream toe



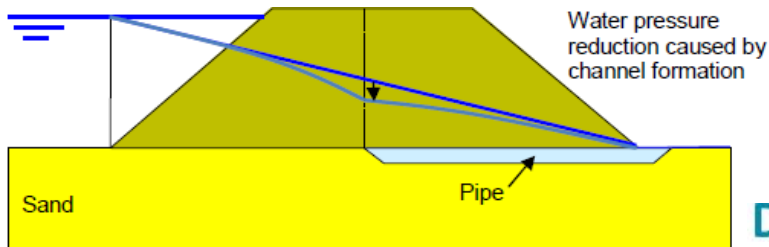
Fiber optic located below upstream membran



Radzicki (2009) , Beck et al. (2010, 2012),



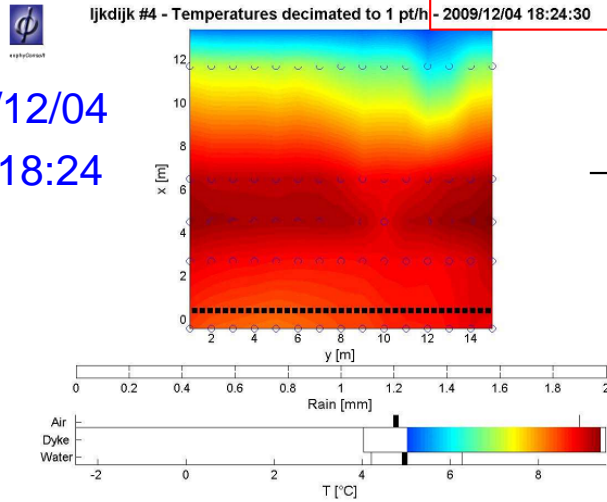
## 2009 IJkdijk test



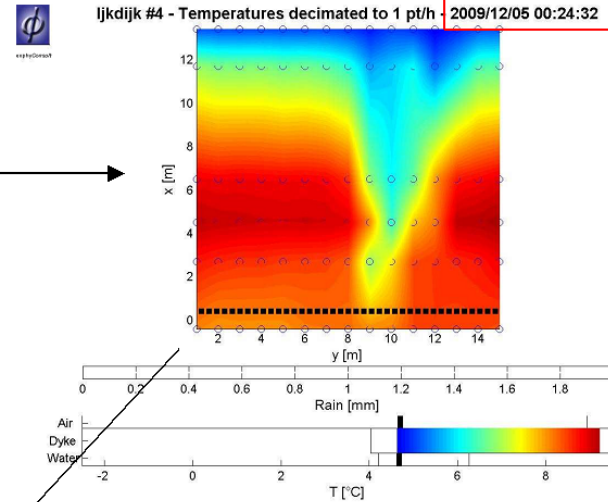
Deltares

## 2009 IJkDijk test

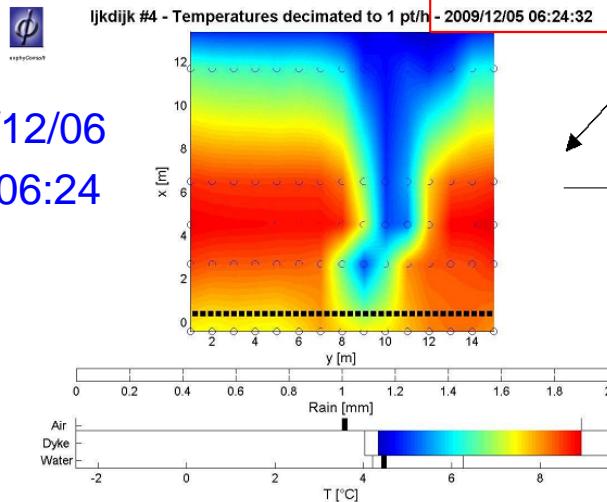
2009/12/04  
18:24



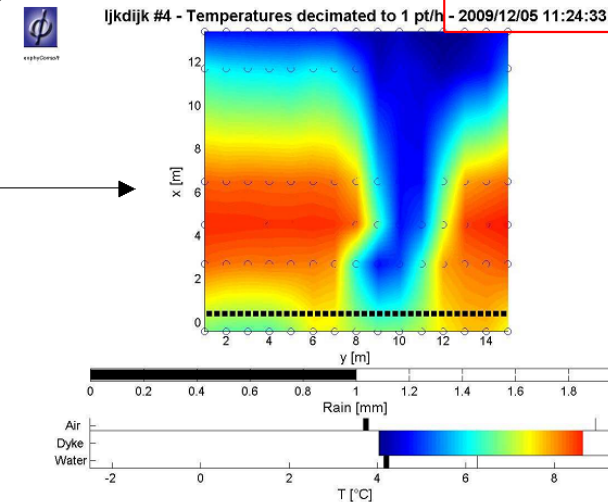
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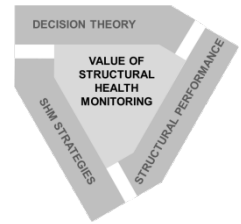


2009/12/06  
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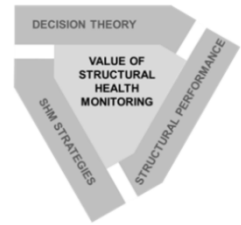
2009/12/06  
11:24





# Models of passive thermal monitoring

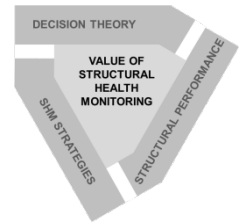
<i>General models division</i>		<i>Signal processing models</i>		<i>Models with the physical meaning of the parameters</i>	
<b>Model name</b>		<b>Daily Analysis Model</b>	<b>Source Separation Model</b>	<b>Impulse Response Function Analysis Models (for example IRFTA model)</b>	<b>Amplitude Model</b>
<b>Minimal period of the temperature data acquisition</b>		about 1 day	about 2-3 months		1 year
<b>Range of the application</b>	<b>Type of the hydraulic structure</b>	Earth dams, dikes of the canals and flood protection levees	Earth dams and dikes of the canals		
	<b>Hydraulic conditions</b>	Saturated and unsaturated zone			Only saturated zone
	<b>Thermal conditions</b>	Analysis in relation to the reservoir temperature and air temperature as well to the other thermal sources.	Analysis in relation to the reservoir temperature and the air temperature.	Analysis only the dam's reservoir temperature influence; air temperature influence must be neglected	
<b>Method principle</b>		Data daily analysis developed using signal analysis methodology	Source separation method	Modelling with an exponential approximation of the impulse response function of the system	Exact solution approximation of the relevant problem for the suffusion layer
<b>Main advantages</b>		The fastest leakage detection method. Possibility of the early warning, automatic leakage detection system installation	Leakage detection method	Parametrical evaluation of the coupled heat and water transport, including leakage detection possibility and its intensity assessment	Seepage velocity estimation in the suffusion layer
<b>Described examples of the model application</b>		Beck et al., 2010	Beck et al., 2010; Cunat, 2012	Radzicki, 2009; Radzicki and Bonelli, 2010; Artières et al., 2007; Cunat, 2012	Johansson, 1997



# Examples of applications

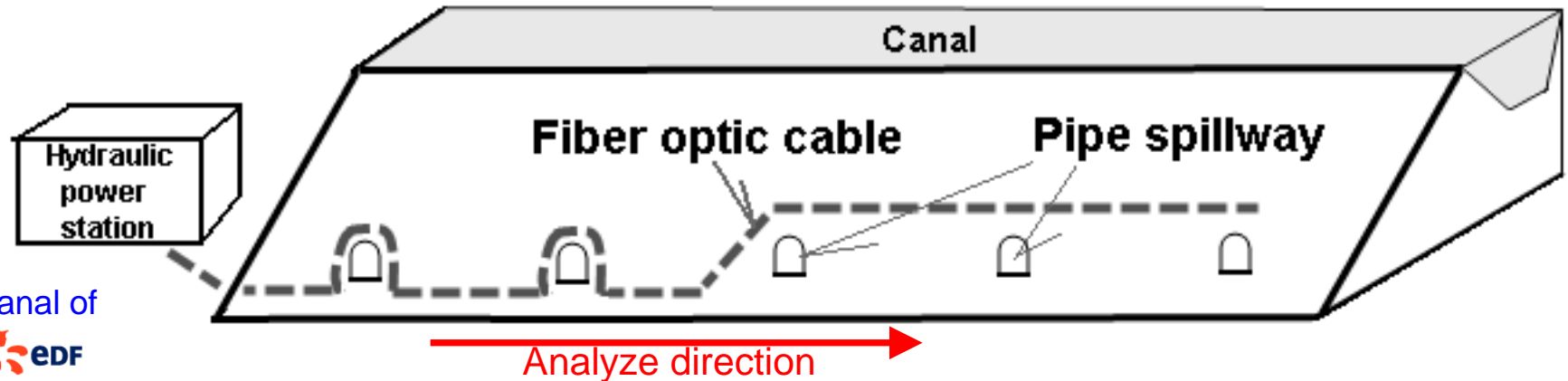
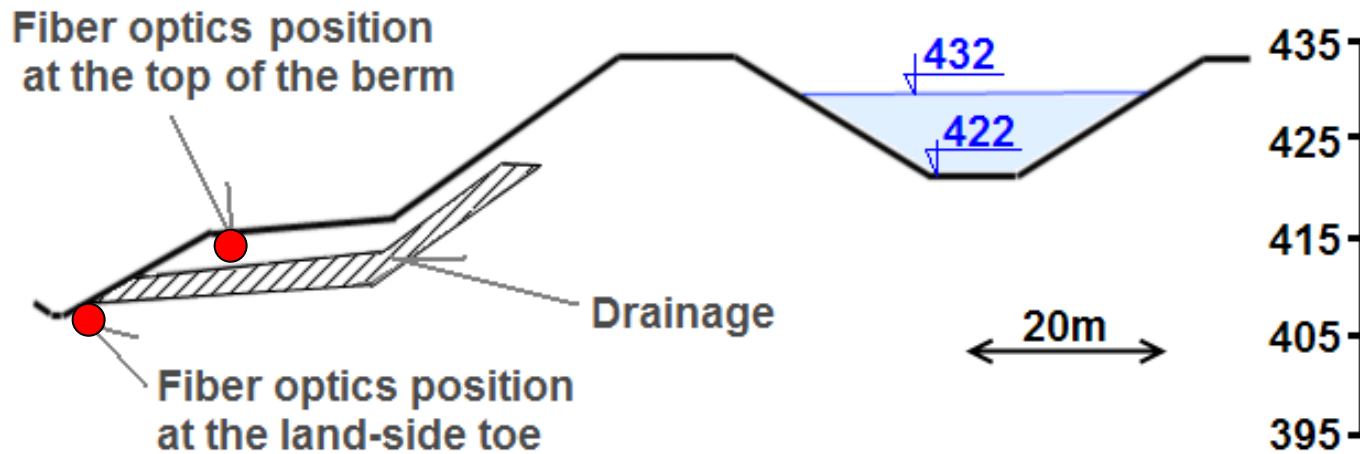
## DIKE OF THE ORAISON CANAL

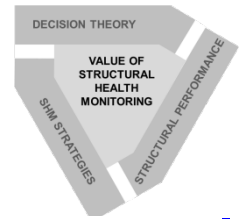




# Examples of applications

## DIKE OF THE ORAISON CANAL

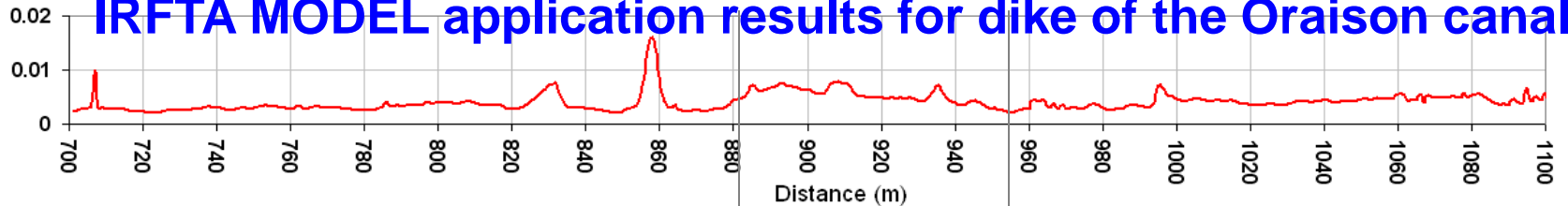




# Examples of applications

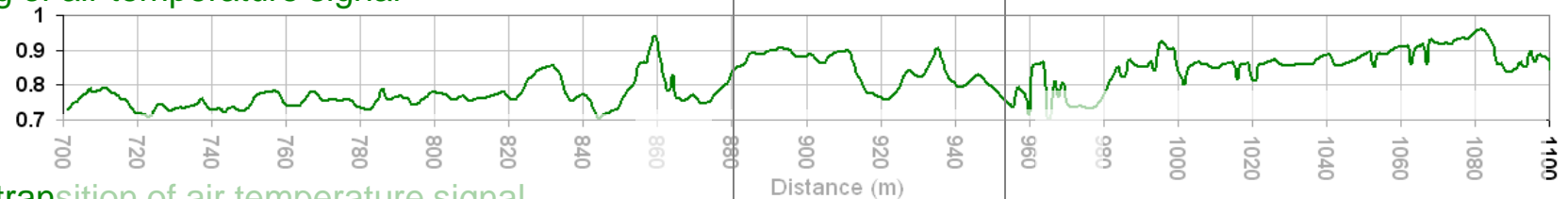
## IRFTA MODEL application results for dike of the Oraison canal

$1-R^2$



Damping of air temperature signal

$\alpha_{pw}$



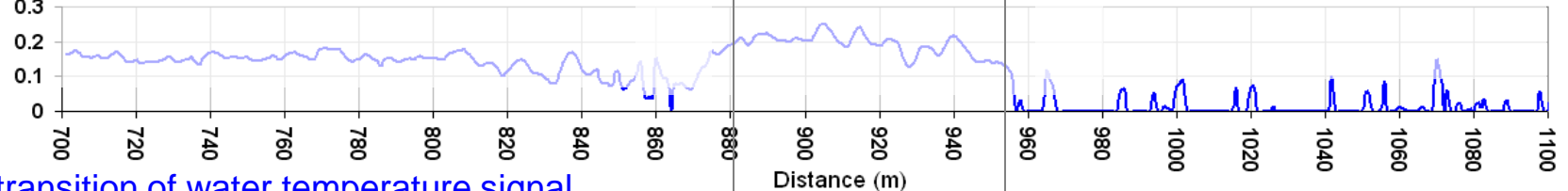
Time of transition of air temperature signal

$\eta_{pw}$  (days)



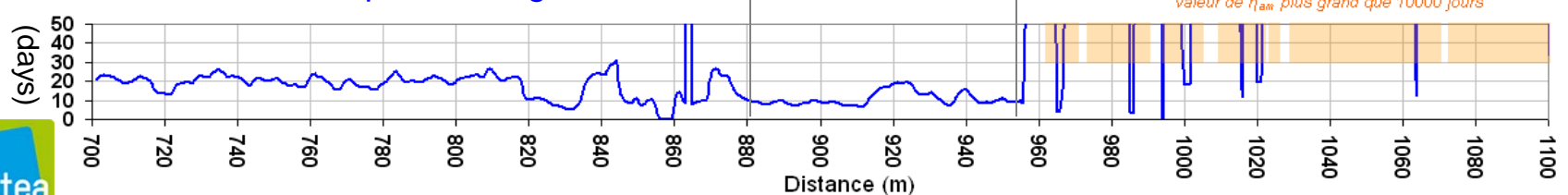
Damping of water temperature signal

$\alpha_{wd}$

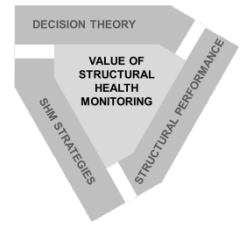


Time of transition of water temperature signal

$\eta_{wd}$  (days)





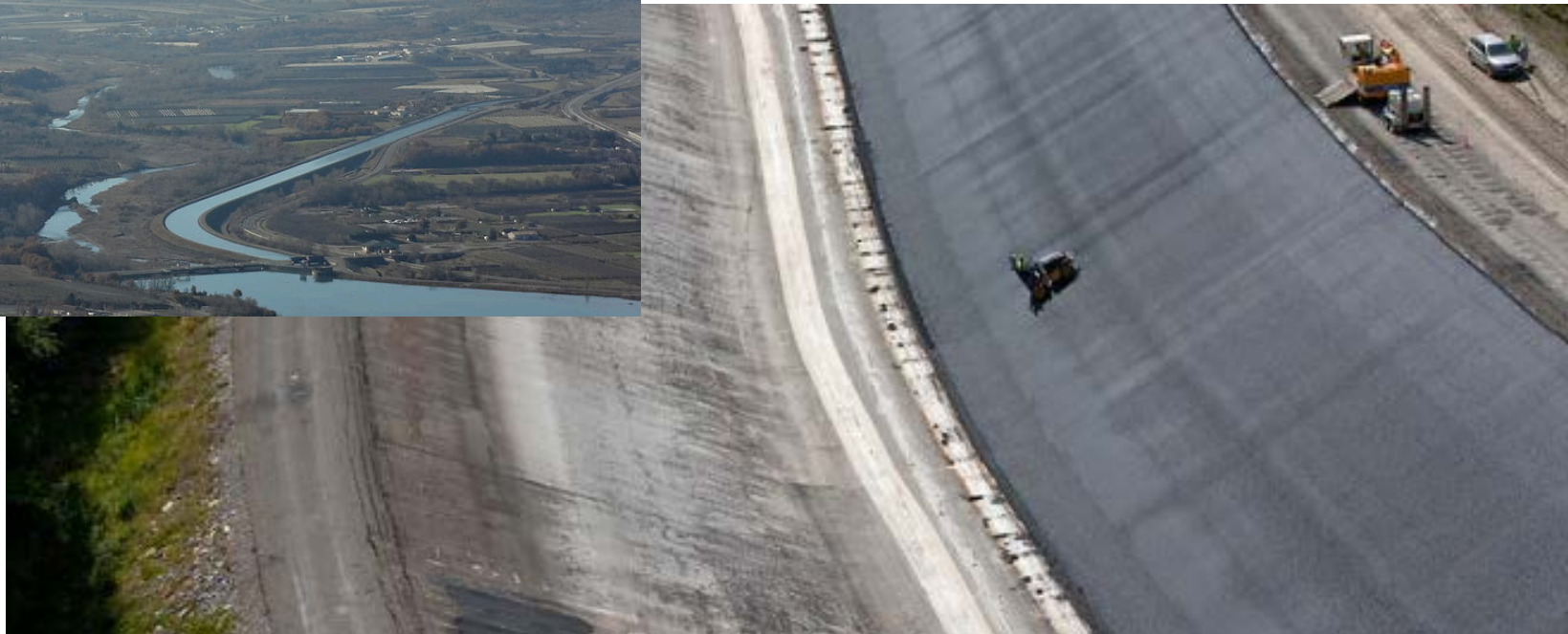


# Examples of applications

## DIKE OF CURBAN CANAL OF DURANCE RIVER

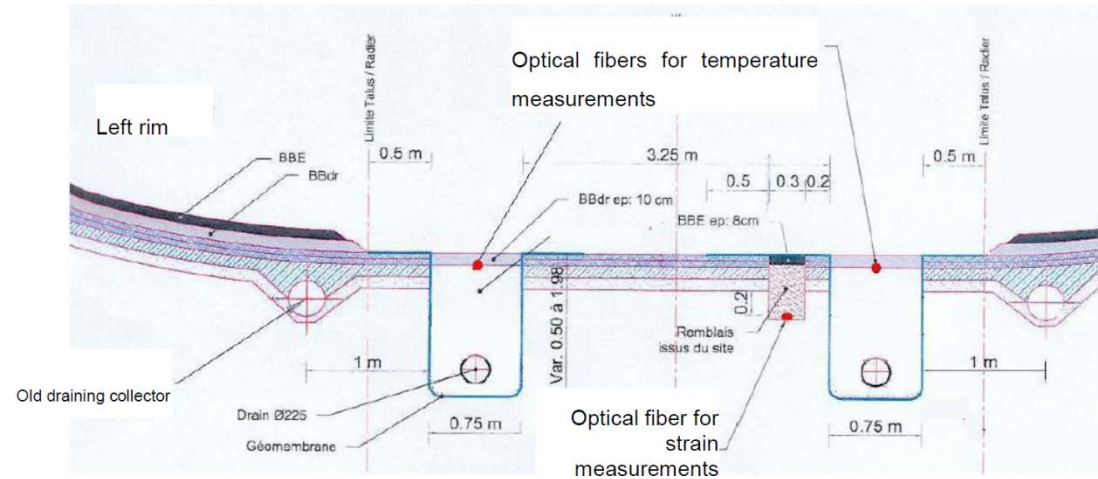
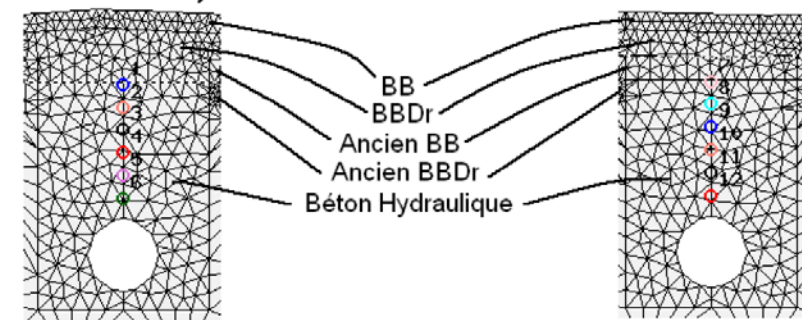
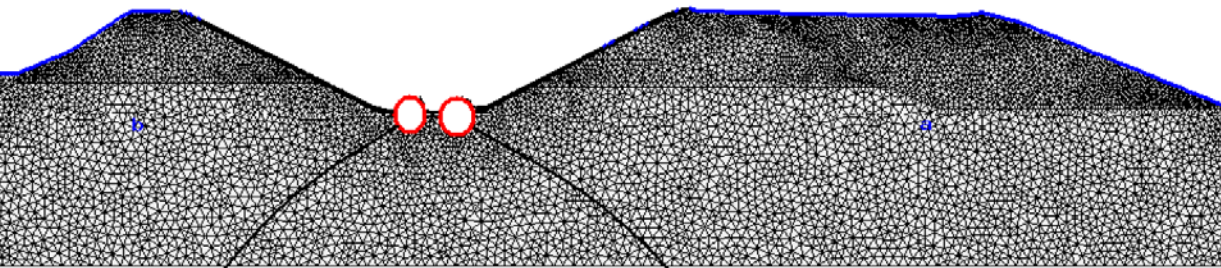


- 5 km of fiber optic

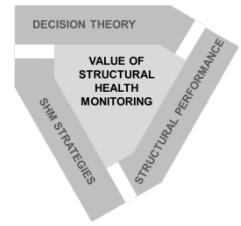


# Examples of applications

## DIKE OF CURBAN CANAL OF DURANCE RIVER

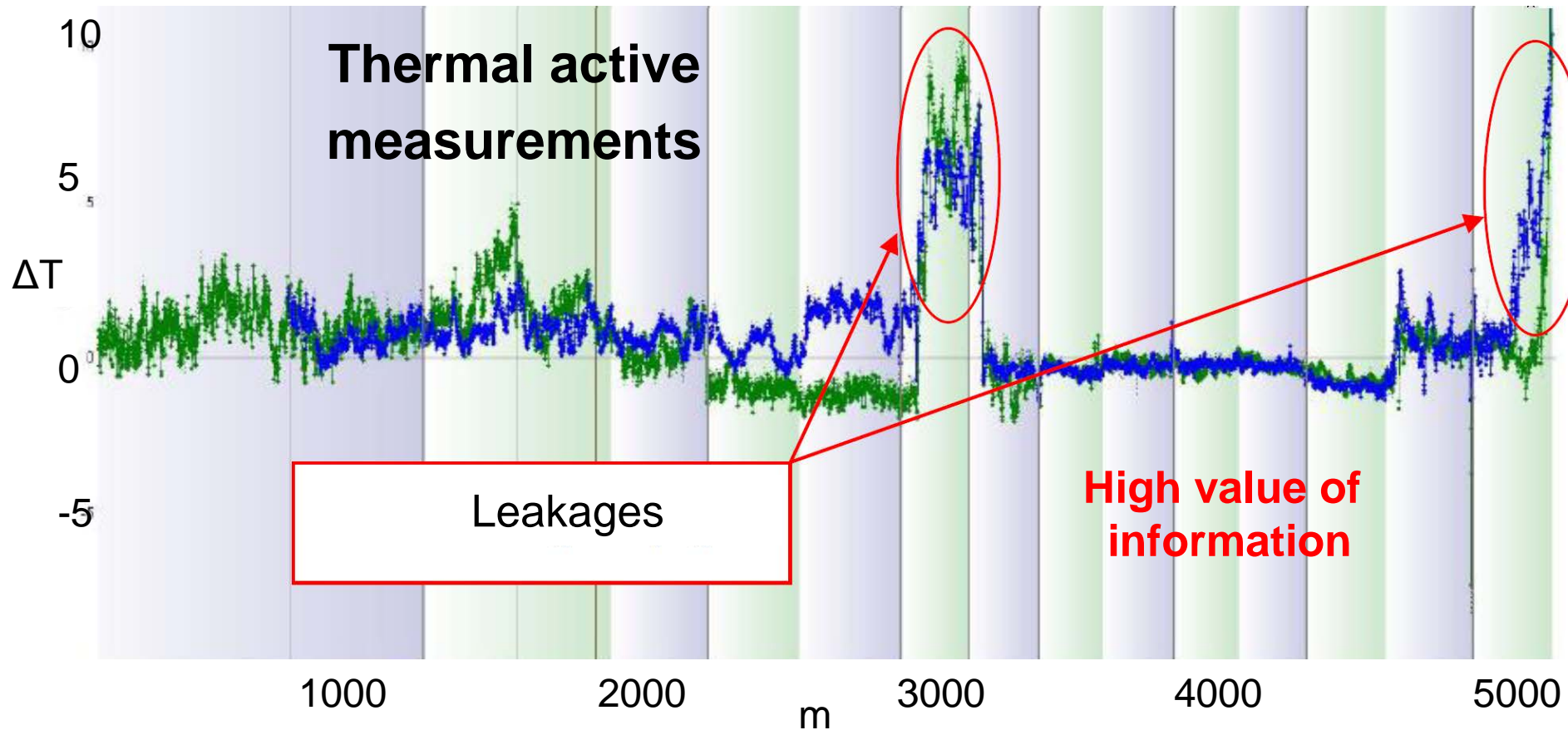


Courivaud et al. (2013)

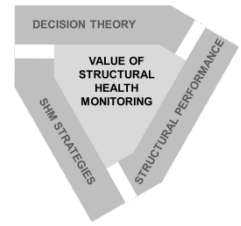


# Examples of applications

## DIKE OF CURBAN CANAL OF DURANCE RIVER



Courivaud et al. (2013)



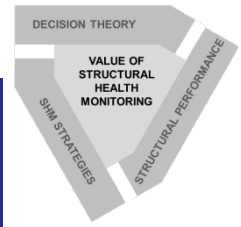
# Examples of applications

## RIGHT LEVEE OF RHINE RIVER

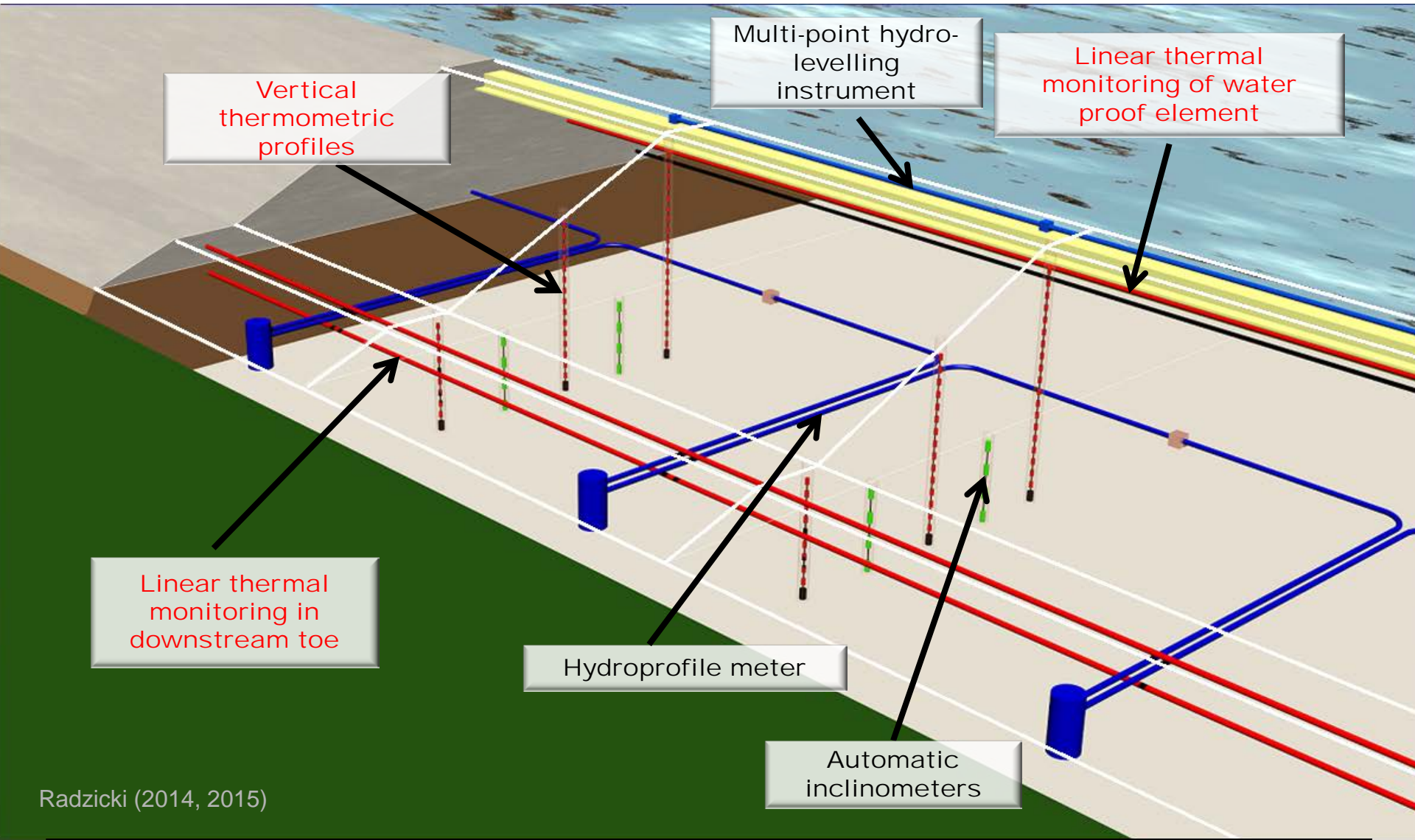


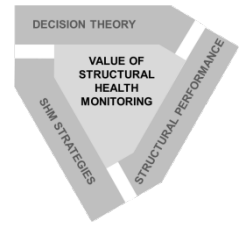
- 38 km of fiber optic

Courivaud et al. (2014)

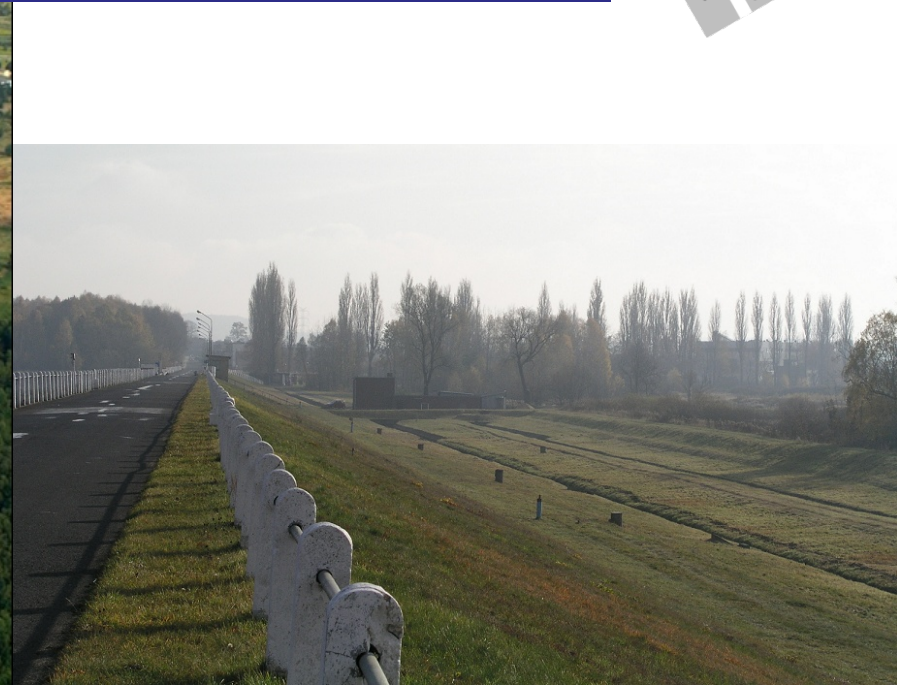


# Quasi 3D thermal monitoring and displacements monitoring

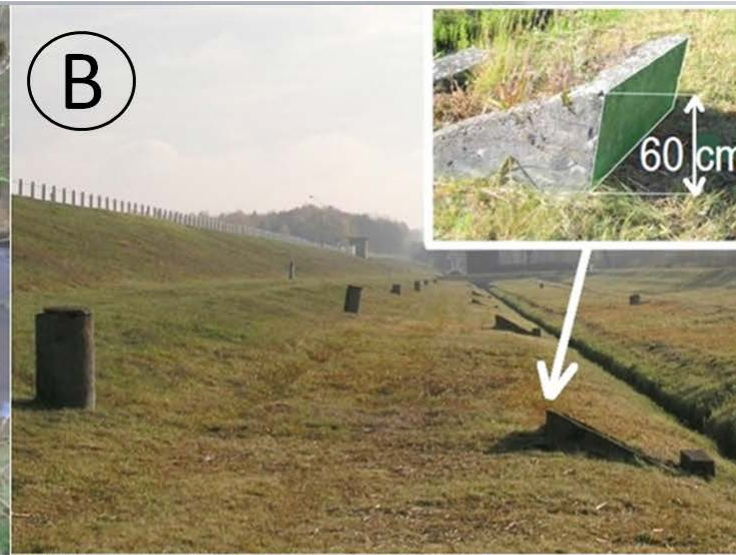




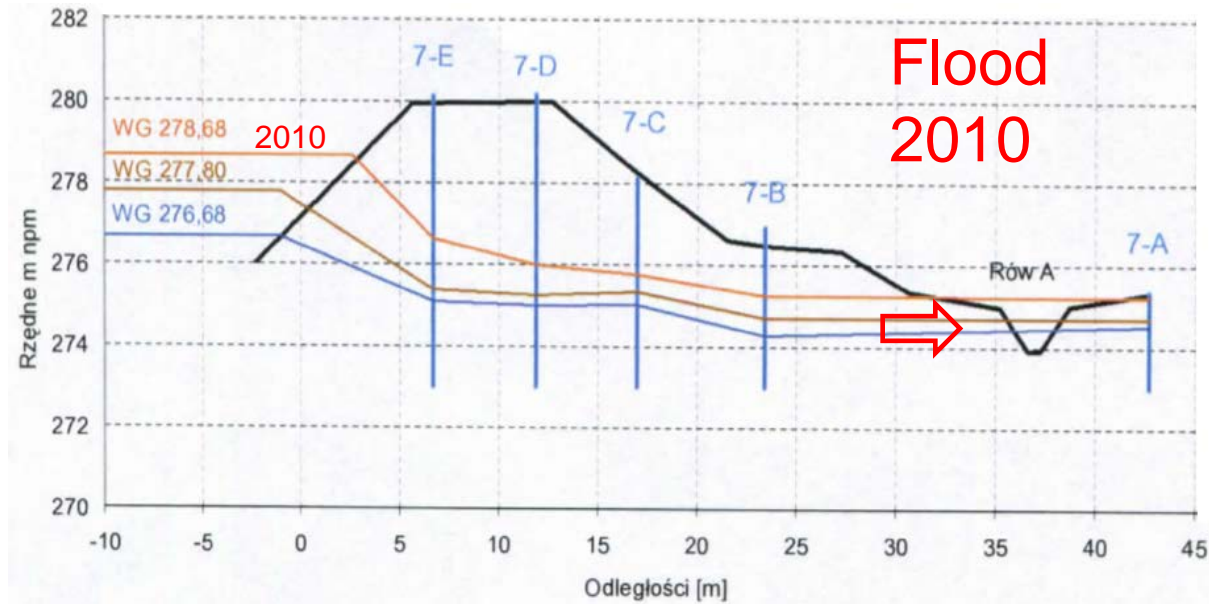
# Kozłowa Góra dam



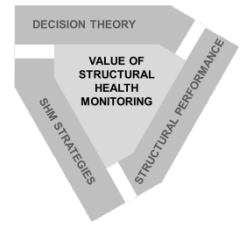
# Kozłowa Góra dam



# Kozłowa Góra dam – flood 2010

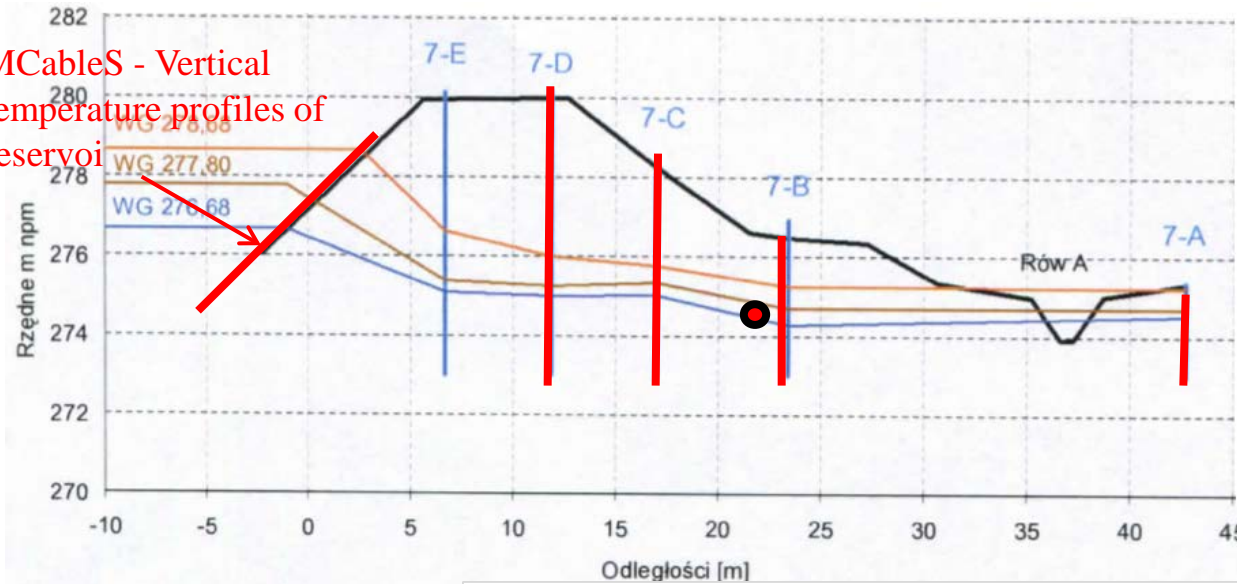




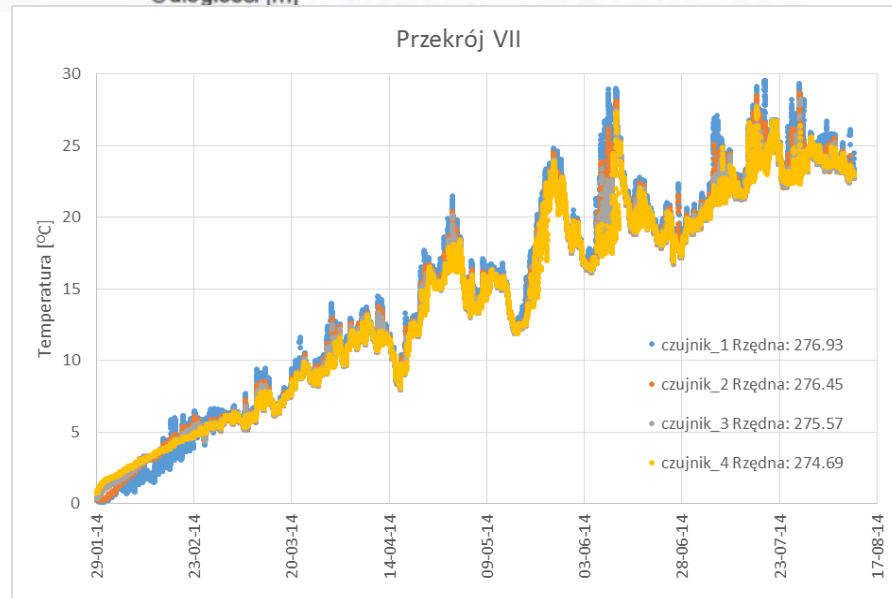


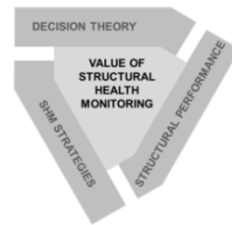
# Kozłowa Góra dam

MCableS - Vertical temperature profiles of reservoir



Cracow University of Technology & Irstea

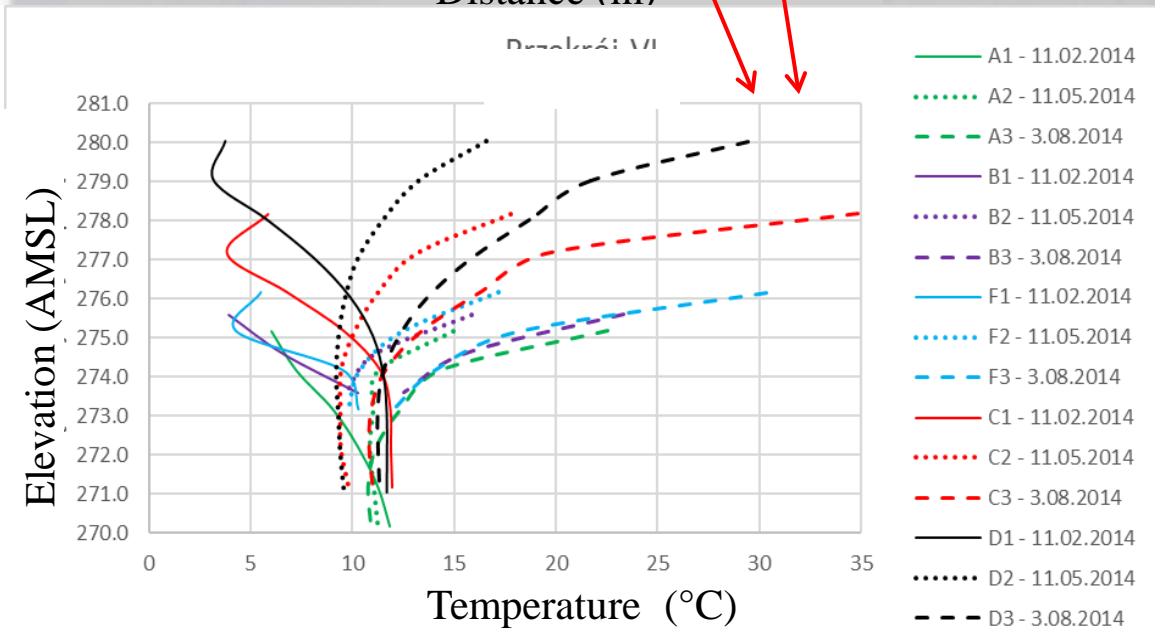
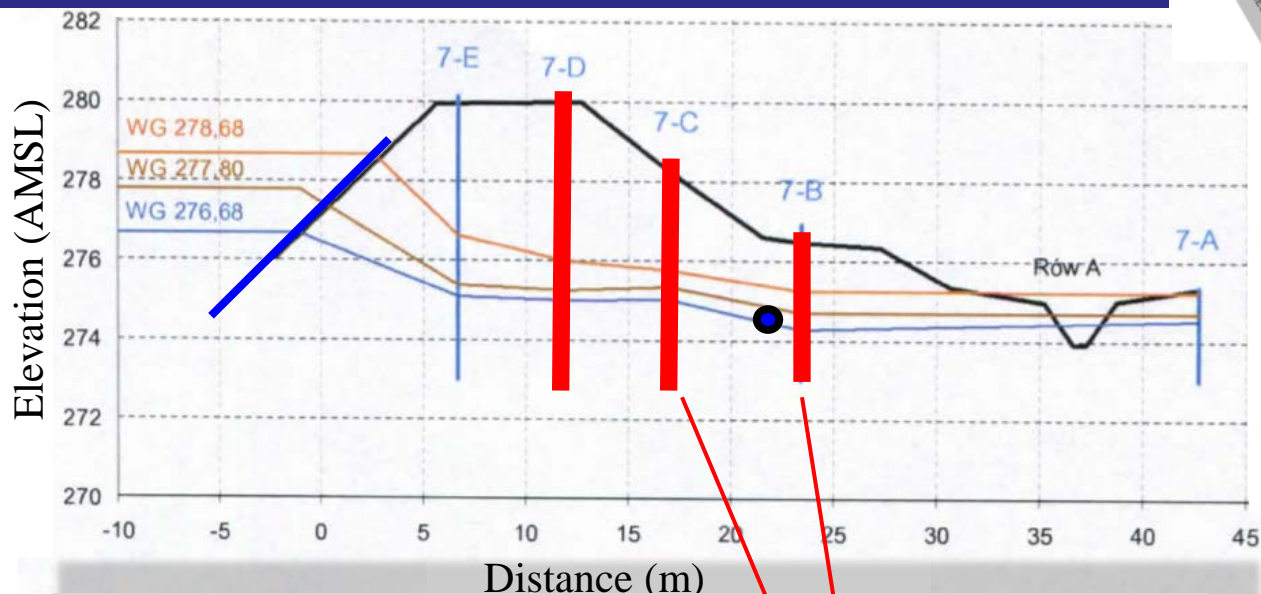




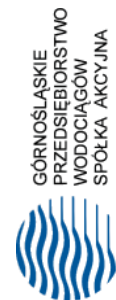
# Kozłowa Góra dam

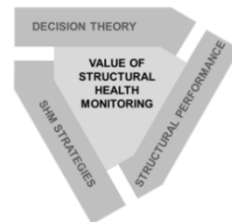
## MCableS

Measurements of vertical temperature profiles in the dam body in existing piezometres



PASSIVE  
THERMAL  
METHOD

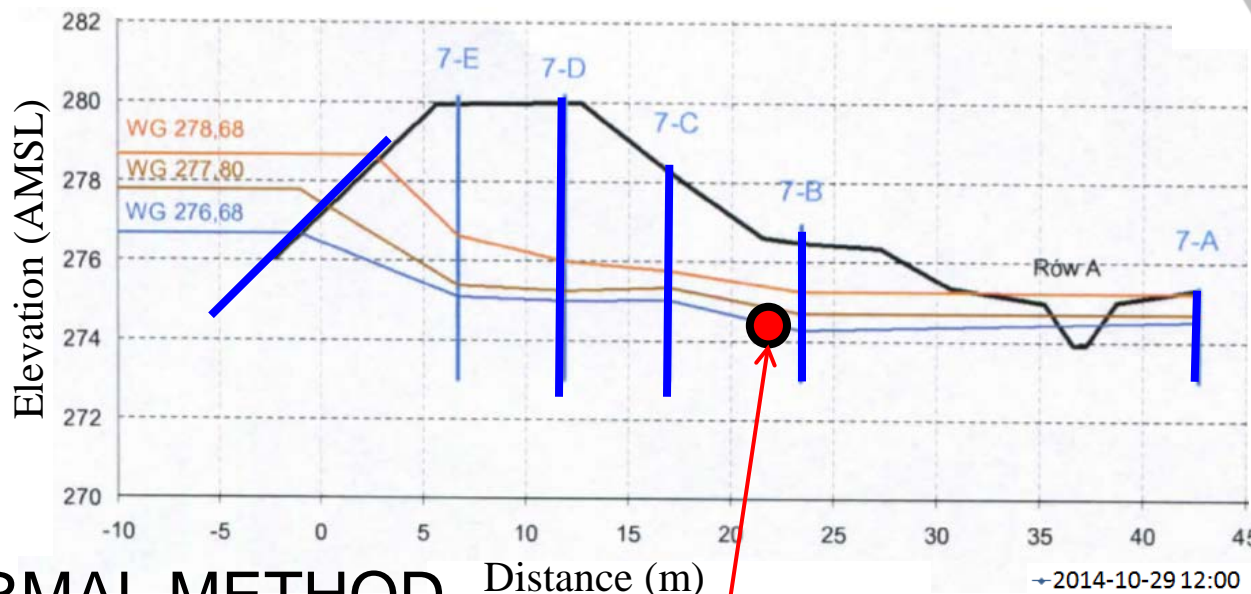




# Kozłowa Góra dam

## MPointS

QUASI LINEAR  
PASSIVE  
temperature  
measurements  
along the dam  
in the  
downstream toe



GÓRNOŚLĄSKIE  
PRZEDSIĘBIORSTWO  
WODOCIĄGÓW  
SPÓŁKA AKCYJNA

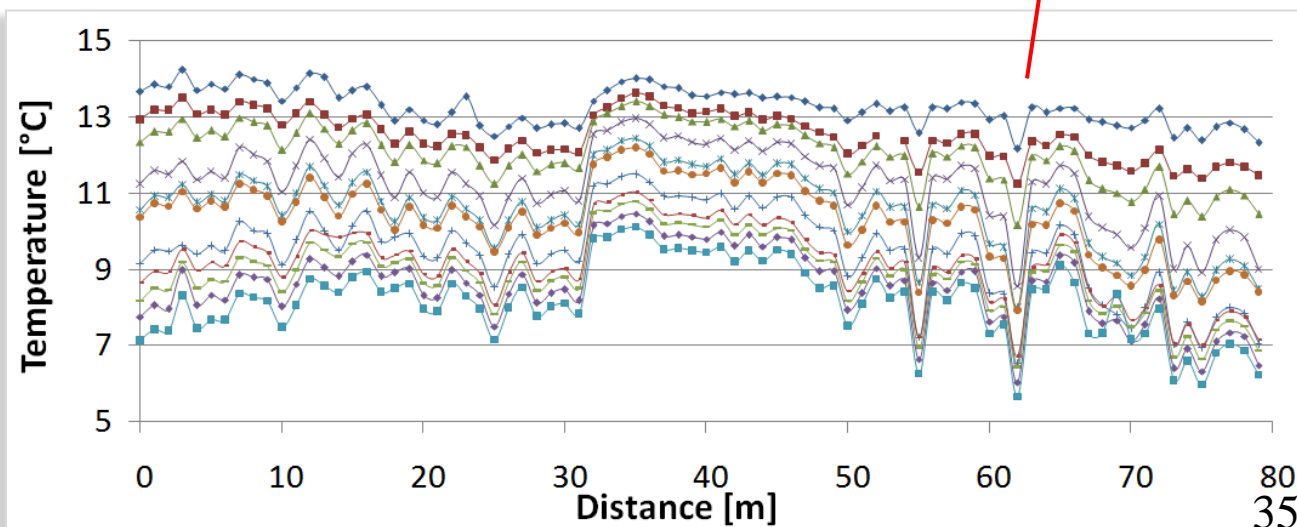


NeoStrain  
Therm3Detect®

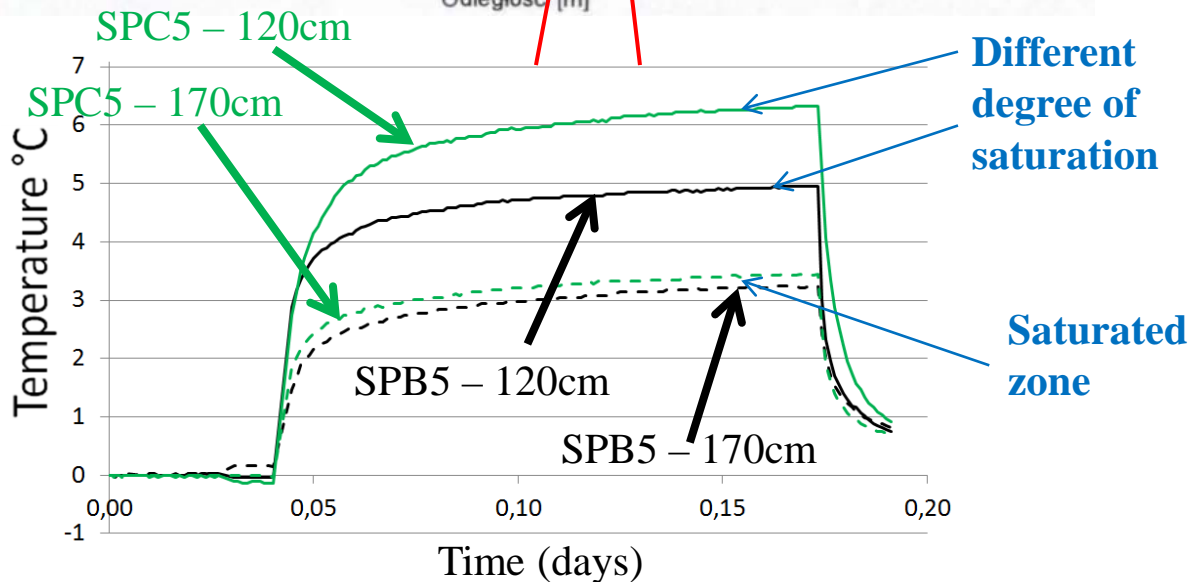
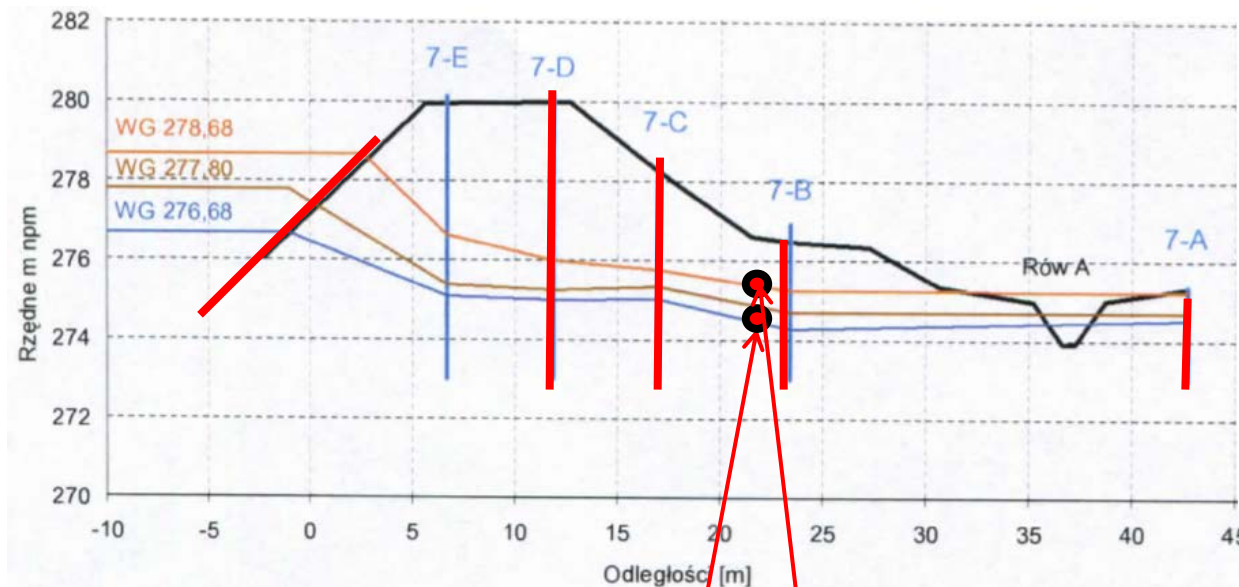
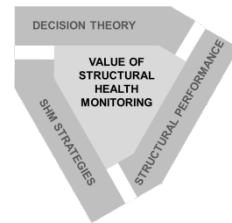


- 2014-10-29 12:00
- 2014-11-08 12:15
- 2014-11-12 12:15
- 2014-11-20 12:00
- 2014-11-26 12:00
- 2014-12-03 12:00
- 2014-12-10 12:00
- 2014-12-17 12:00
- 2014-12-24 12:15
- 2015-01-02 12:30
- 2015-01-07 12:00
- 2015-01-28 12:00
- 2015-02-04 12:00
- 2015-02-11 12:00
- 2015-02-18 12:00
- 2015-02-25 12:15
- 2015-03-04 12:15
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- 2015-03-18 12:15
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- 2015-04-01 11:45
- 2015-04-08 12:15

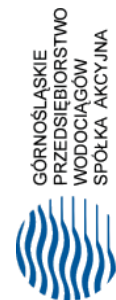
## PASSIVE THERMAL METHOD



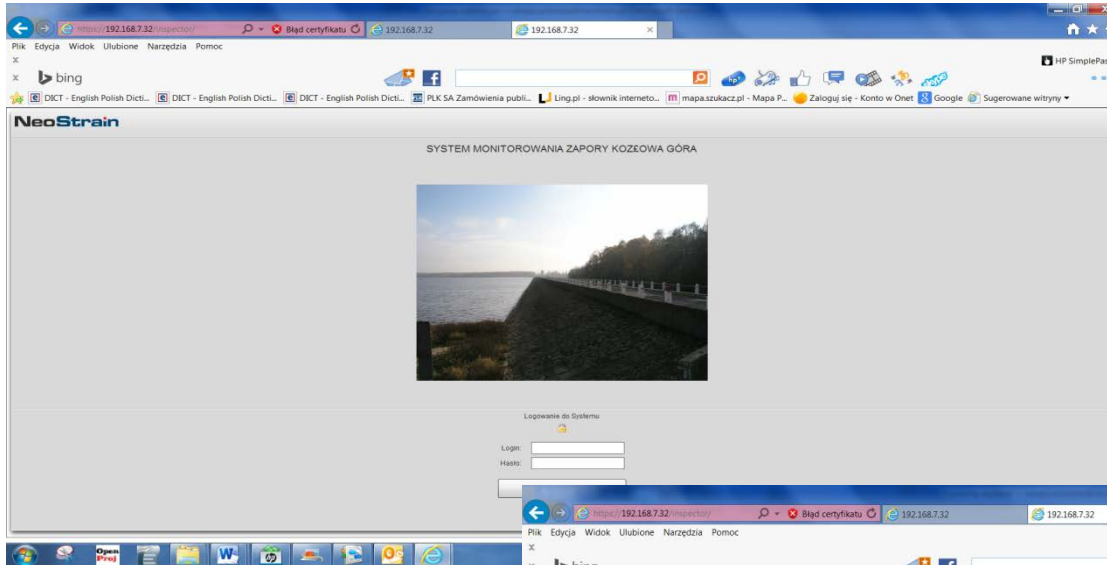
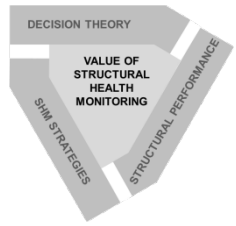
# Kozłowa Góra dam



ACTIVE  
METHOD



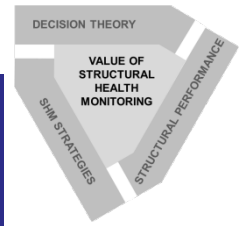
## Kozłowa Góra dam



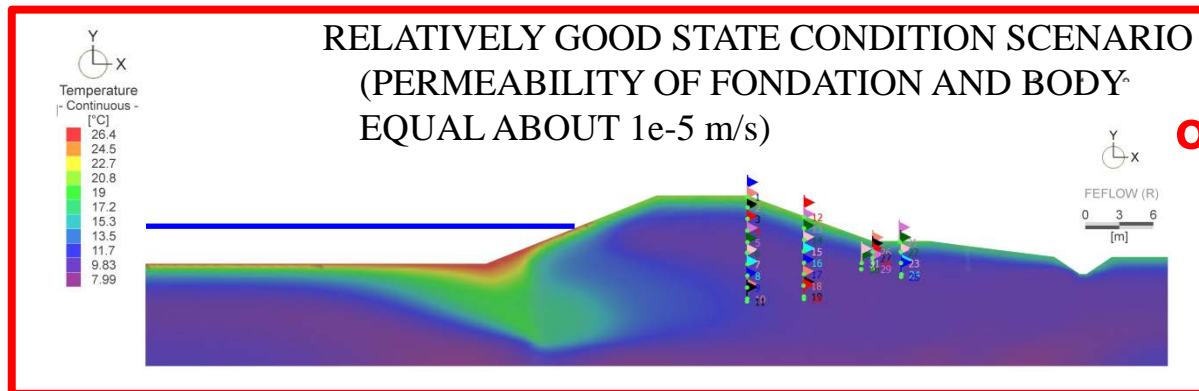
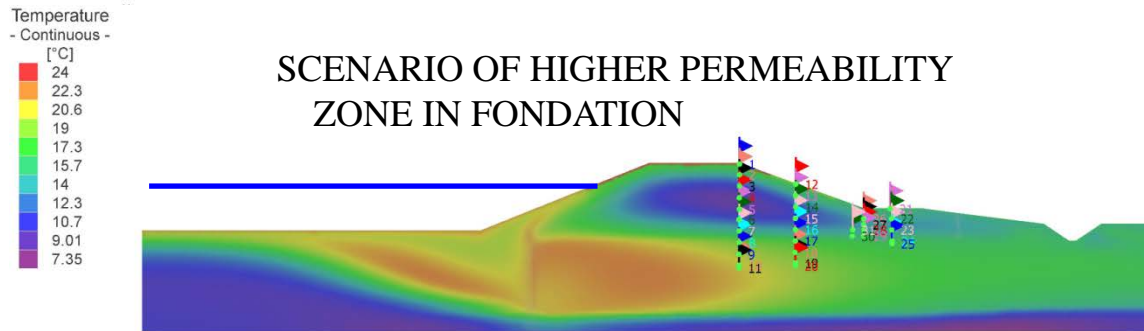
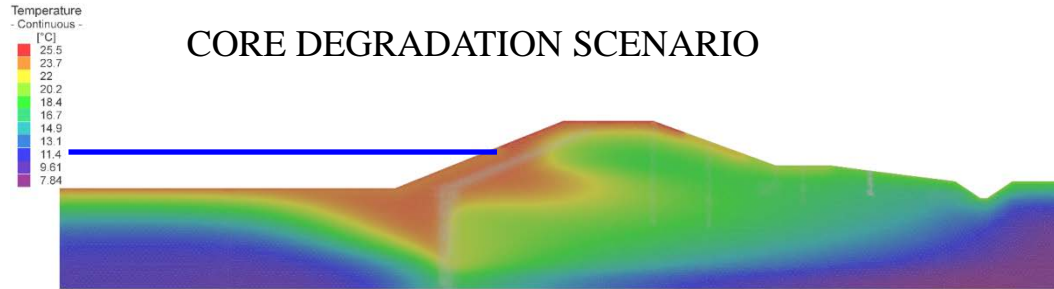
Nazwa	Adres	SAD	Typ	Trend	Jednostka	Min		Max		Max.min	Średnia	Aktualna
						Wartosc	Próg	Wartosc	Próg			
Ciśnienie	P-6a-P	SAD0			Pa	136145.16	---	138719.75	---	2574.59	137451.03	138502.67
Ciśnienie	P-7a-P	SAD0			Pa	118153.91	---	120339.94	---	2686.03	119526.73	118480.86
Ciśnienie	P-7c-P	SAD0			Pa	163229.82	---	165909.77	---	2679.95	164602.65	163559.48
Ciśnienie	P-7b-P	SAD0			°C	111971.17	---	114685.77	---	2714.60	113380.63	112295.85
Temperatura	P-16-P	SAD0			°C	11.22	---	11.42	---	0.20	11.32	11.23
Temperatura	P-1c-P	SAD0			°C	16.52	---	16.72	---	0.20	16.62	16.53
Temperatura	P-1f-P	SAD0			°C	8.11	---	8.20	---	0.09	8.15	8.19
Temperatura	P-1b-P	SAD0			°C	7.87	---	8.06	---	0.12	7.93	7.96
Temperatura	P-6d-P	SAD0			°C	16.21	---	16.49	---	0.29	16.35	16.21
Temperatura	P-6c-P	SAD0			°C	16.43	---	16.71	---	0.28	16.57	16.44
Temperatura	P-6f-P	SAD0			°C	9.41	---	9.51	---	0.10	9.47	9.42
Temperatura	P-6b-P	SAD0			°C	9.67	---	9.82	---	0.14	9.76	9.67
Temperatura	P-6a-P	SAD0			°C	11.05	---	11.10	---	0.05	11.08	11.08
Temperatura	P-7d-P	SAD0			°C	16.42	---	16.84	---	0.43	16.63	16.42
Temperatura	P-7c-P	SAD0			°C	16.39	---	16.64	---	0.26	16.49	16.40
Temperatura	P-7b-P	SAD0			°C	7.59	---	8.03	---	0.44	7.78	8.03
Temperatura - sensor 1	P-16-P	SAD0			°C	12.34	---	12.65	---	0.31	12.59	12.34



# Kozłowa Góra dam – NUMERICAL MODELLING



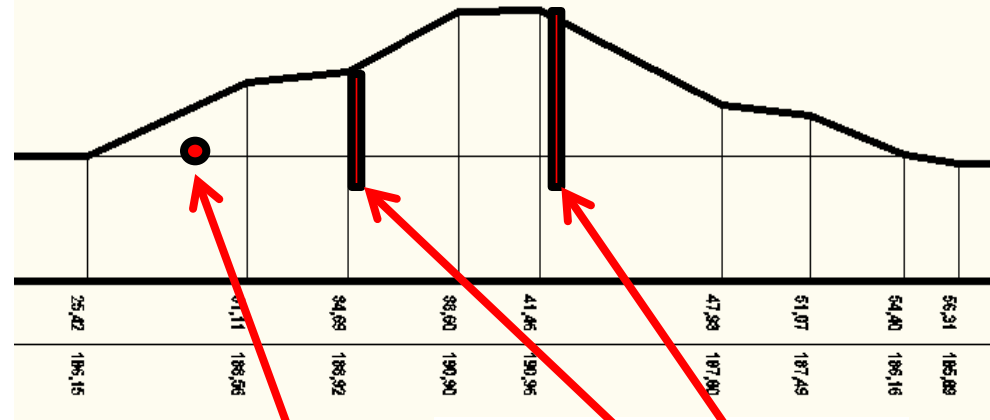
Intermediate results  
of research carried  
out by:  
K.Radzicki  
P.Opaliński  
S.Bonelli



High  
value of  
information,  
low cost  
of the solution

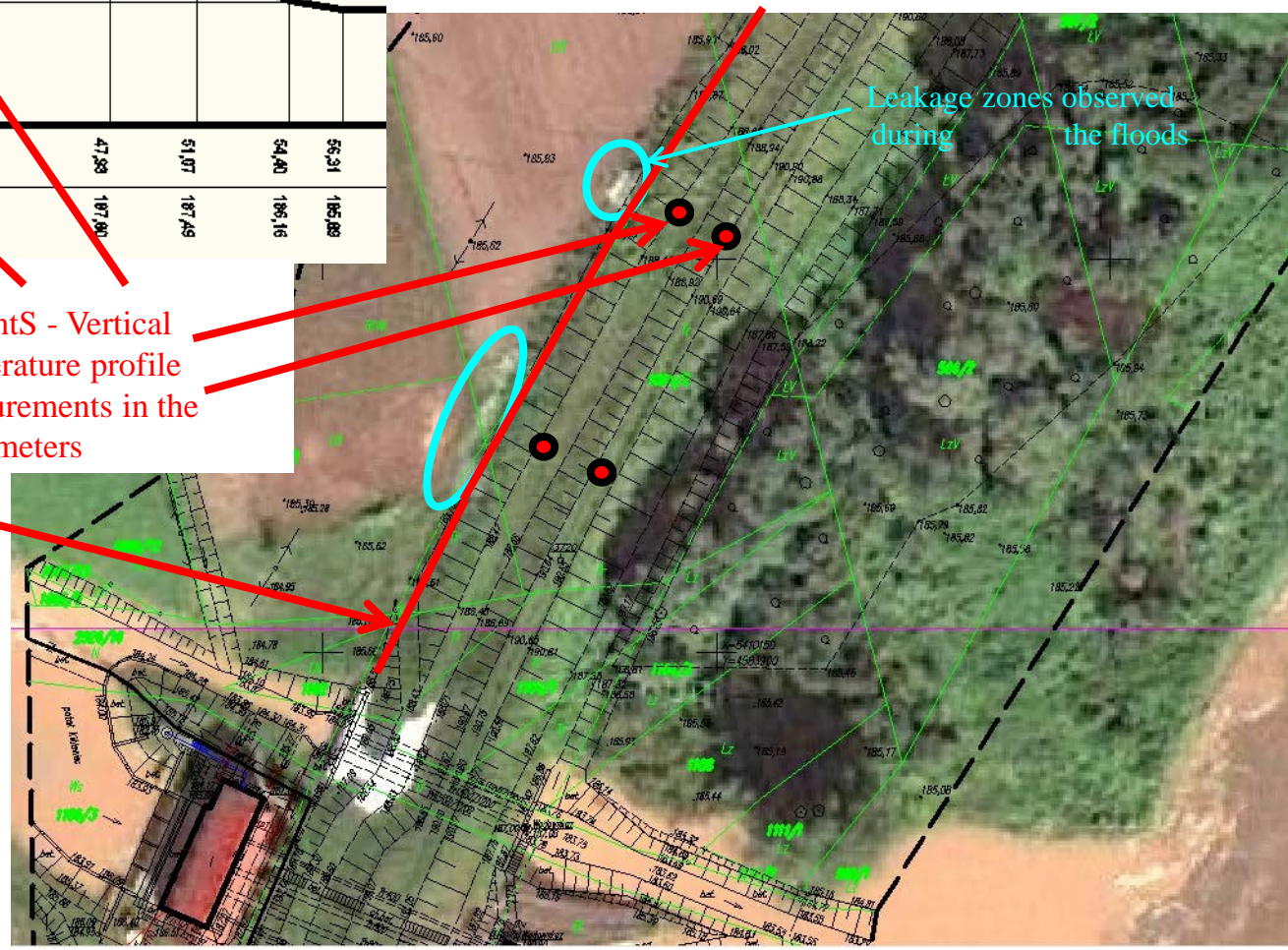


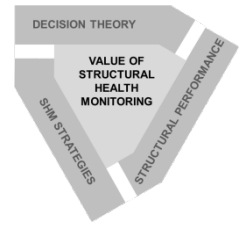
## The first levee in Poland instrumented in thermal monitoring system including linear thermal monitoring – 2016



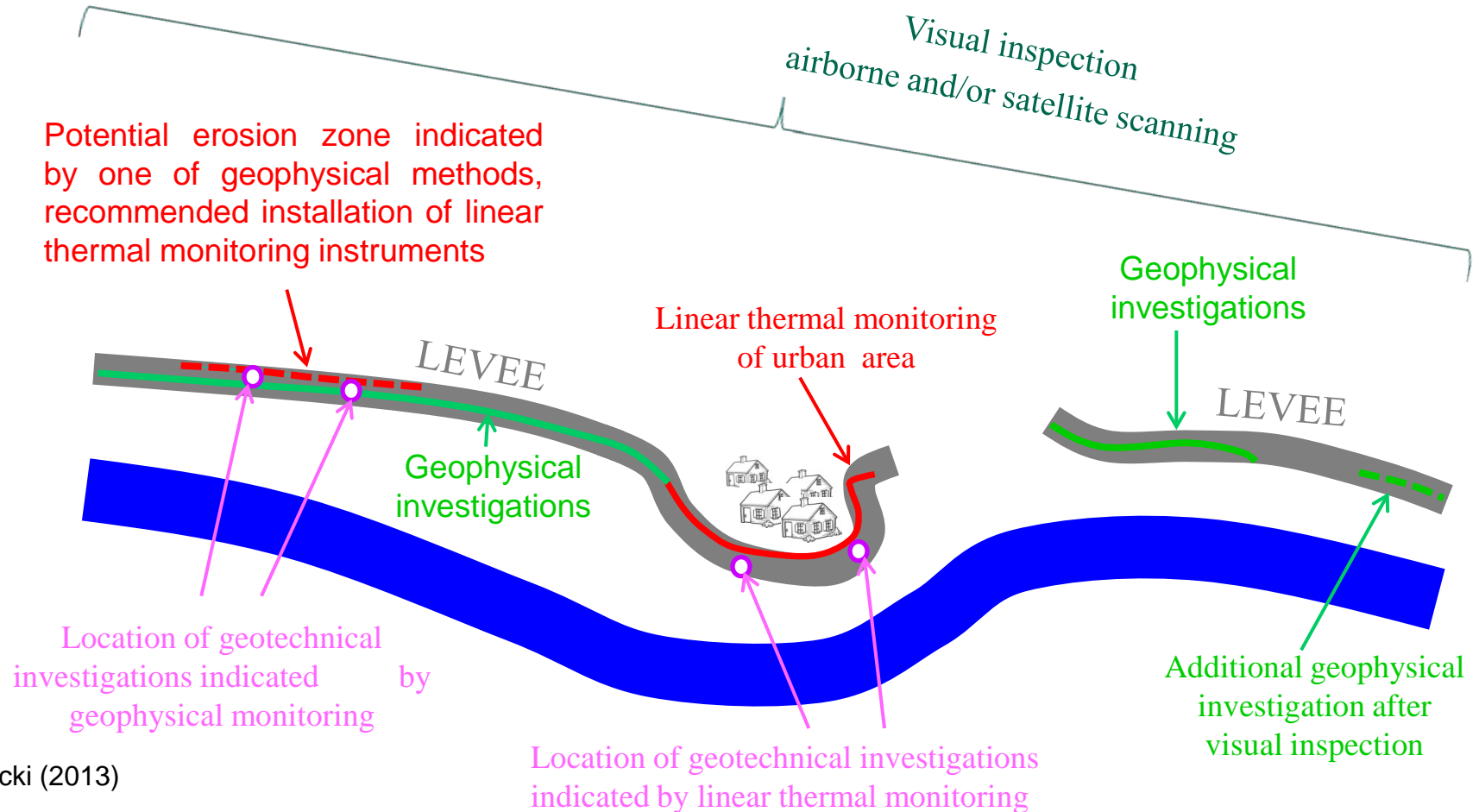
MPointS – Quasi linear temperature measurements in downstream toe

MPointS - Vertical temperature profile measurements in the piezometers



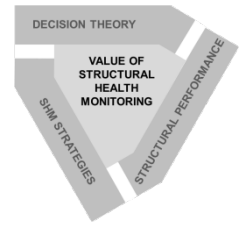


# Example of methodology of levees state assessment



Radzicki (2013)



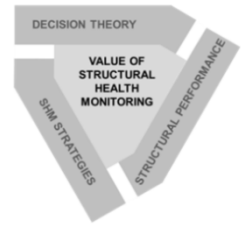


## KEY FEATURES OF THERMAL MONITORING METHOD

- MONITORING OF LEAKAGES AND INTERNAL EROSION PROCESSES IS CONTINUOUS ALONG DAMMING CONSTRUCTION
- EARLY DETECTION OF LEAKAGES AND INTERNAL EROSION PROCESSES
- IT ALLOWS TO EVALUATE DYNAMIC OF THE PROCESSE AND SPATIAL DYSTRICTION OF LEAKAGES AND INTERNAL EROSION PROCESSES
- POSSIBILITY OF AUTOMATIC DETECTION OF LEAKAGE AND THE RISK OF EROSION

## APPLICATION RESULTS OF THERMAL MONITORING

- MINIMIZATION OF THE FAILURE PROBABILITY DUE TO THE DEVELOPMENT OF INTERNAL EROSION (PIPING ESPECIALLY) AND/OR LEAKAGE
- MINIMIZATION OF THE SCOPE AND COSTS OF RENOVATION THROUGH ACCURATE DIAGNOSIS AND RELIABLE ASSESMENT OF DYNAMIC AND SPATIAL DYSTRICTION OF LEAKAGES AND INTERNAL EROSION PROCESSES



Thank you for your attention

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