

Evaluating the value of SHM with longitudinal performance indicators and hazard functions using Bayesian dynamic predictions

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- 1. Objectives of evaluating the value of SHM
- 2. Joint model of longitudinal data and hazard function
- 3. Hazard based maintenance planning and value of SHM
- 4. Conclusions



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Monitoring or not?





What's the difference?



Evaluating the Value of SHM (VoSHM)





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Longitudinal data and hazard function



Predict risk of death for a patient with same disease.

Historical PI measurements Structural Engineering of a group of structures/components Datasets from simulation Or



Hazard function

Longitudinal data and hazard function

1) Structural performance time series

 $y(t) = m(t) + \epsilon(t)$

m(t) ~ the underlying structural state with random effects b ~ variance D. $\epsilon(t)$ ~ observation error, N(0, σ_1)

2) Survival process defining the hazard function $h(t) = \lim_{s \to 0} \frac{Pr(t < T < t + s | T > t)}{s}$ $= h_0(t) \exp\{\alpha^T f(b, t)\} + \alpha_n\}$ $h_0(t)$ ~baseline hazard α ~regression parameters.



Baseline hazard and association structure

> Baseline hazard $h_o(t)$:

Weibull baseline →accelerated failure time model

Association structure:

m(t) and it's time dependent changing rate m'(t) $h(t) = \sigma_2 t^{\sigma_2 - 1} \exp\{\alpha_1 m(t) + \alpha_2 m'(t) + \alpha_3\}$



Parameter estimation $\theta = [\sigma_1, \alpha_1, \alpha_2, \alpha_3, \sigma_2, D)$

- > Sample dataset $\boldsymbol{b}(u_0, D) \rightarrow \{\boldsymbol{y}_i, T_i\}, \ \boldsymbol{y}_i = [y_{it}], \ \begin{cases} t = 1 \sim ni \\ i = 1 \sim N \end{cases}$
- $\succ \quad p(y_i, T_i, \delta_i | b_i, \theta)$

$$= \prod_{l=1}^{n_i} p(y_{il} | b_i; \theta_y) p(T_i, \delta_i | b_i; \theta_l) p(b_i; \theta_b)$$

$$\propto \left[(\sigma_{1}^{2})^{-\frac{n_{i}}{2}} \exp\left\{-\sum_{l} (y_{il} - m_{i}(l))^{2} / 2\sigma_{1}^{2}\right\} \times [\sigma_{2} t^{\sigma_{2}-1} \exp\{\alpha_{1} m_{i}(T_{i}) + \alpha_{2} m_{i}'(T_{i}) + \alpha_{3}\}] \right] \times \exp\left[-\int_{0}^{T_{i}} \sigma_{2} t^{\sigma_{2}-1} \exp\{\alpha_{1} m_{i}(s) + \alpha_{2} m_{i}'(s) + \alpha_{3}\}ds\right] \times p(b_{i}; \theta_{b})$$



Parameter estimation

Likelyhood :
$$L(\mathbf{D}|\theta) = \prod_{i=1}^{N} [p(y_i, T_i, \delta_i | b_i, \theta)]$$

Prior : $\pi(\theta)$
Posterior : $\pi''(\theta) \propto L(\mathbf{D}|\theta)\pi(\theta)$
 $= \prod_{i=1}^{N} [p(y_i, T_i, \delta_i | b_i, \theta)] \pi(\theta)$

MCMC methods: Gibbs sampler, MH algorithm

R package: JMbayes



Joint modeling



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Value of SHM

- Z Inspection outcome;
- X Monitoring outcome;
- Θ Structural state $\leftarrow f'_{\Theta}(\theta)$;
- *a* Maintenance action, d(e, z);
- e Inspection decision $\leftarrow h(t) \& h(t)^T$





Value of SHM

For M₀:
$$E'_{\Theta}[C_T(e,d,\theta)] = \int_{\Theta} C_T(e,d,\theta)f'_{\Theta}(\theta)d\theta$$

For M₁: $E''_{\Theta}[C_T(x,e,d,\theta)] = \int_{\Theta} C_T(x,e,d,\theta)f''_{\Theta}(\theta|x)d\theta$

EVSI: $E_X[CVSI(x)] = E'_{\Theta}[C_T(e, d, \theta)] - \int_X E''_{\Theta}[C_T(x, e, d, \theta)] f_X(x) dx$ (VoSHM)

For X: $f_X(x|M) = E_{\Theta}[f_X(x|M,\theta)]$

Model uncertainty Measurement uncertainty



Expected TLCC

 $E[C_T(e, d, t_{SL})] = E[C_F(e, d, t_{SL})] + E[C_I(e, d, t_{SL})] + E[C_R(e, d, t_{SL})] + E[C_M(e, d, t_{SL})]$

$$E[C_{F}(e, d, t_{SL})] = \sum_{t=1}^{t_{SL}} \left[\left(1 - \sum_{i=1}^{t-1} p_{R}(e, d, i) \right) \frac{1}{(1+r)^{t}} \left(h(e, d, t) \left(1 - p_{F}(e, d, t-1) \right) C_{F} + p_{R}(e, d, t) E[C_{F}(e, d, t_{SL} - t)] \right) \right]$$

+ $p_{R}(e, d, t) E[C_{F}(e, d, t_{SL} - t)] \right]$
{SL} - service life, r - discount rate. $C{F}, C_{Insp}, C_{R}, C_{M}$

Straub, D. (2004). Generic Approaches to Risk Based Inspection Planning for Steel Structures. ETH Zürich. Thöns, S. (2012). Monitoring based condition assessment of offshore wind turbine support structures. ETH Zürich.

Aspects to calculate expected TLCC

Probabilities related to the decision tree:

•
$$p_{F}(t) = \begin{bmatrix} 1 - \exp\left[-\int_{0}^{t} \sigma_{2} t^{\sigma_{2}-1} \exp\{\alpha_{1} m_{i}(s) + \alpha_{2} m_{i}'(s) + \alpha_{3}\}ds\right] \end{bmatrix}$$

Weibull distribution

•
$$p_{_{det}} = \Phi\left(\frac{\delta(t) - \delta_{0.5}}{\sigma_{0.5}}\right)$$
 $\delta_{0.5}, \sigma_{0.5} \rightarrow \text{quality of inspection}$

•
$$p_R = \left(\frac{\delta(t)}{\delta_{max}}\right)^{r_a}$$
 ($\delta(t) \le \delta_{max}$) r_a decision parameter

Barone, G. and Frangopol, D. M. (2013). Hazard-Based Optimum Lifetime Inspection and Repair Planning for Deteriorating Structures



Aspects to calculate expected TLCC

Risk acceptance criteria and decision rules:

 $h_{max} \rightarrow$ Maximum allowable yearly failure rate (JCSS)

Threshold approach \rightarrow inspection planning

 $h(t)^T \leq h_{max}$





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- A joint modeling of time dependent structural performance and hazard function is first introduced;
- Derived hazard function is used as a tool for determining inspection/repair plans;
- The uncertainties related to the SHM outcomes are considered and incorporated in the joint model, leading to an updated inspection/repair planning and expected TLCC;
- The difference between the prior and posterior expected TLCC is defined as the VoSHM.



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Thank you for your attention!





